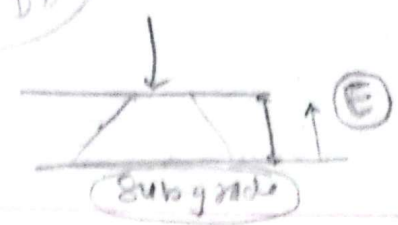


DMC & DD



Pavement

→ A relatively stable layer with even surface, constructed over the natural soil for the movement of traffic.

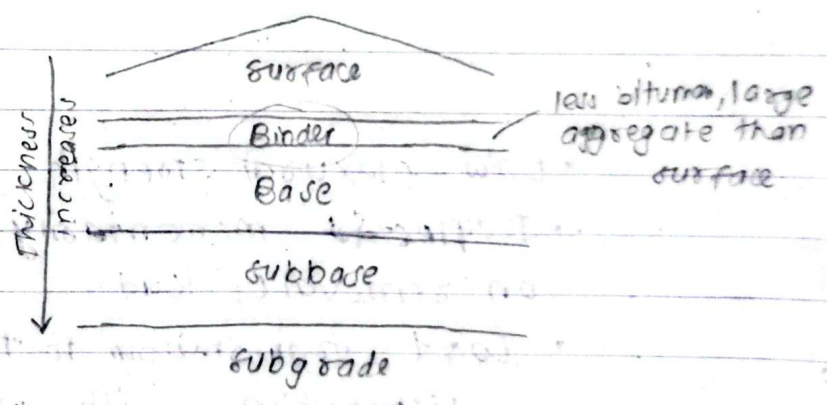
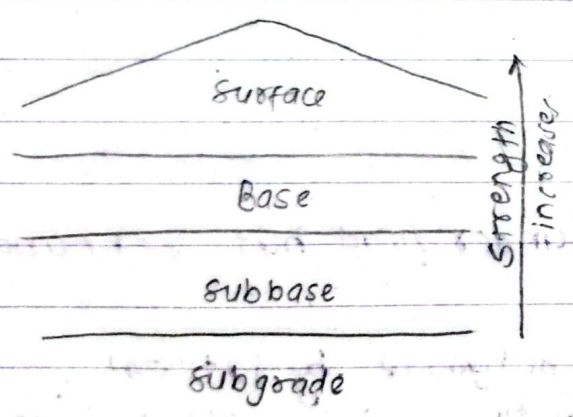
→ Functions:-

- To support and distribute wheel load of vehicle over a wide underlying area of subgrade soil.
- To keep the temporary deformation within the permissible range.

Pavement layers:-

Indian Practice

American Practice



base/sub-base → made using aggregate/granulars

↳ distribute wheel load evenly to underlying layers

→ Subgrade should have CBR value of 5% minimum. If not, it is increased by soil stabilization.

*Types of pavement:

Depending on structural behaviour:

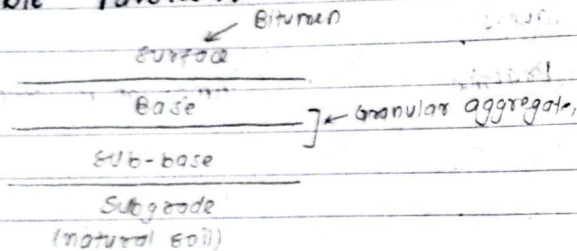
(i) Flexible pavement → grain to grain

(ii) Rigid Pavement → Slab

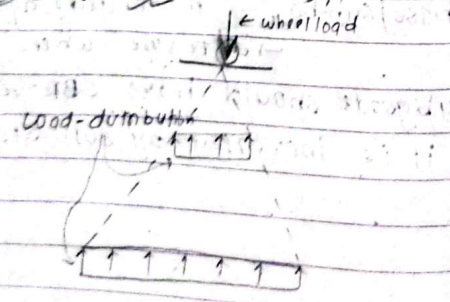
(iii) Semi-rigid Pavement → fly ash aggregate

(iv) Composite Pavement

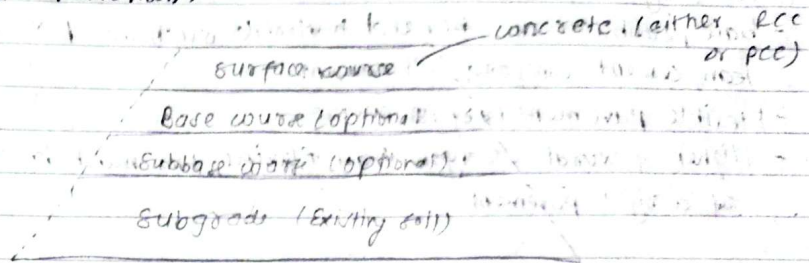
(i) Flexible Pavement



- Low-flexural strength
- Deflected momentarily under load but rebounds on removal of load
- Load transmission to the subgrade by lateral distribution with grain to grain point of contact
- Designed in layers, empirical method



(ii) Rigid Pavement



- Joints are given & seen in plan in transverse & longitudinal direction to counteract the shrinkage properties of concrete.
- Mud pumping + frost action are seen due to poor joints! To prevent them, a granular layer is preferred b/w surface & subgrade layers.

[Mud pumping → joint वाट Mud सहितको पानी निस्को
 Frost action → पानी जम्ने रज layer (surface & subgrade) छिचका

- Cem. concrete slab
- High flexural strength
- Load distribution by slab action
- Permanent settlements
- Design by structural analytical techniques



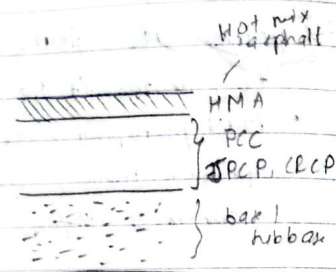
→ stage construction not possible in flexible pavement

(iii) Semi-rigid Pavement

- base, subbase of bonded materials such as pozzolanic cement lean cement concrete, soil cement.
- Flexible pavement surface course.
- Higher flexural strength than flexible but much lower than that of a rigid pavement.

(iv) Composite Pavement

- Ideal pavement
- PCC bottom layer, HMA top layer.
- Very expensive, rarely used in new construction.
- Mostly rehabilitation of PCC using asphalt overlays.

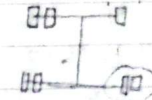


□ Loads and other factors controlling Pavement Design.

1. Traffic and loading factors
2. Material properties
3. Environment factors
4. Failure criteria

1. Traffic & loading factors.

- Axle load
- Number of load repetitions.
- Contact area
- Vehicle speed.



ii Axle load

- total wt. of the vehicle carried by its axles
- Axle load → wheel load → pavement surface.

Wheel load:

- Higher the wheel load, thicker is the pavement required.
- Pavement design is governed by number and wheel loads of the commercial vehicles.

Wheel configuration:

- Most commercial vehicles are provided with dual rear wheels
- Affect the stress distribution and deflection

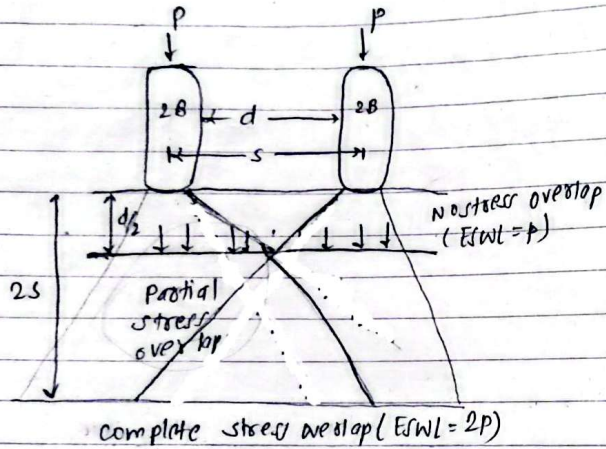
→ Design:

Flexible pavement: wheel on only one side is considered.

Rigid pavement: wheel on both side are considered.

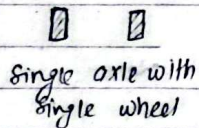
load \rightarrow grain to grain laterally distributed.

\rightarrow Dual wheel load is converted into equivalent single wheel load to simplify the analysis.

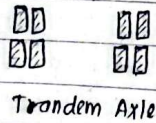


• Axle configuration:

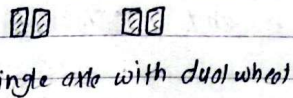
\rightarrow commercial vehicles are provided with multiple axles to further enhance the load carrying capacity.



Single axle with single wheel



Tandem Axle



Single axle with dual wheel



Tandem Axle

(E_{swl}) \times 2 \times 2 \times use 80kN
or load 80kN

• In design standard axle load and Equivalency factor (F) are used

Equivalency factor for an axle load L (F)

$$= \frac{\text{Damage caused by passage of axle load } L \text{ on a pavement}}{\text{Damage caused by passage of}}$$

Axle load

\rightarrow Generalized ~~low~~ version of AASHTO's Fourth power damage formula:

structural damage caused by an axle load varies as fourth power of its ratio to the standard axle load.

• Equivalency factor for an axle load L (F) = $\left(\frac{L}{L_s}\right)^4$

Empirical relation & varies for different failures

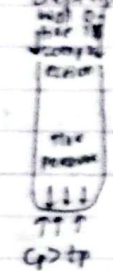
material property

□ Number of load repetitions

- Repeated application of the wheel load → pavement distress → pavement failures
- total number of repetitions of the axle loads is computed as cumulative number of standard axle for design life.

□ Contact area

- wheel load is assumed to be uniformly distributed over the contact area.
- size depends on the contact pressure.



Low pressure tire



High pressure tire

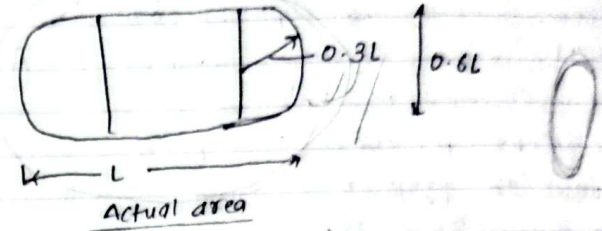
(Normally truck in high pressure) (commercial)

→ True shape is elliptical
Flexible pavement:

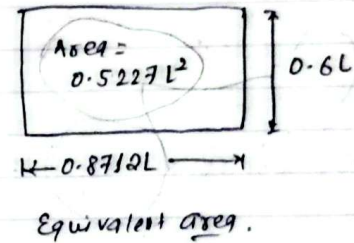
→ Each tire is assumed to have a circular contact area.

Rigid pavement:

→ Elliptical shape with a rectangular and two semicircles is assumed.



→ For FEM analysis, an equivalent rectangular area is assumed.



□ Vehicle speed

- More speed Less pressure.
- Low speed High pressure.

→ directly related to duration of loading.

2. Material Properties:

- Must be specified to determine pavement responses (stress, strain and displacement)
- Linearly elastic: Elastic moduli and Poisson's ratio
- For consideration of moving load / repetition of load, resilient modulus is a better representative.
- Nonlinear property property of material can be characterized by a stress dependent resilient modulus.

3. Environmental Factor

- Temperature
- Precipitation
- Road Geometry (small effects)

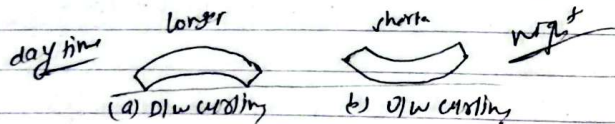
Temperature

Both temp & ppt. affect elastic moduli

Flexible pavement

Rigid pavements:

- create curling stress and affect slab subgrade contact and the stress values.
- Determine joint and crack openings and affect the efficiency of load transfer



• Frost Penetration:

- Temp. effect

Precipitation

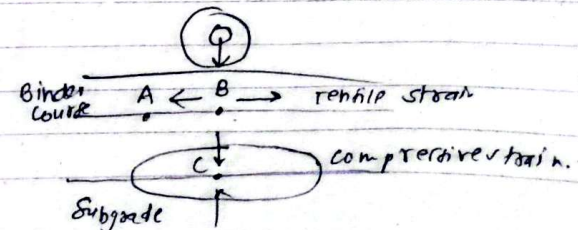
- Quantity of surface water infiltration affects the moisture content of the subgrade and depth of GWT.
- Poor drainage may bring lack of shear strength, pumping, loss of support etc.

4. Failure Criteria:

- Number of failure criteria is adopted considering different distress types.

Flexible pavement

- Fatigue cracking.
- Under repeated traffic loading, bituminous surface of pavement displays flexural fatigue cracking.
- Failure criteria: Relates allowable number of load repetitions to the tensile strain at the bottom of the bituminous layer based on laboratory fatigue test



- rutting (erfardh)
 - surface depression (rut depth) along the wheel path.
 - Failure criteria.
 - ① Limit vertical compression strain on

- Thermal cracking
 - Low temperature cracking
 - Thermal fatigue cracking.
 - Mix stiffness & fracture strength relationship to temperature, tensile strain due to daily temp. cycle.

- Pumping, faulting / spalling / joint deterioration
 - ↳ concrete & soil interaction
 - difficult to analyse mechanically

Design Methods for flexible pavements:

- Mechanistic method
- Semi-empirical method
- Empirical Method
- Mechanistic-empirical method.

Mechanistic Method

- Boussinesq's theory
 - A layer theory first derived by Joseph Valentin Boussinesq.

Assumptions:-

- ↳ Homogenous
- ↳ Isotropic
- ↳ Ideally elastic (constant elastic parameters E and μ -)
- ↳ Semi-infinite

$$\text{vertical stress } (\sigma_z) = p \cdot \left[1 - \frac{z^3}{(a^2 + z^2)^{3/2}} \right]$$

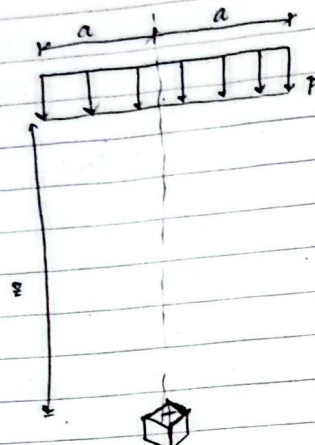
(due to UDL on circular area)

a → radius of circular loaded area
 p → applied pressure per unit area
 z → depth.

$$\text{vertical displacement } (\Delta) = \frac{pa}{E} \times F$$

E → Modulus of elasticity of soil
 F → Deflection factor for poisson's ratio of soil $\mu = 0.5$

• vertical displacement due to u.d.l acting on a circular plate of radius a at depth z on another axis passing through center of plate



$$\Delta = \frac{pa}{E} F, \quad F = \text{deflection factor}$$

For flexible plate

$$F = \frac{3}{2} \times \frac{1}{\left(1 + \frac{z^2}{a^2}\right)^{3/2}} \quad (\mu = 0.5)$$

$$\Delta_{max} = \frac{1.5pa}{E} \quad \text{For } z=0$$

• rigid plate,

$$\Delta_{max} = \frac{1.18pa}{E}$$

$$\Delta = f(p, a, E, z)$$

$$\Delta = \frac{pa}{E} \times \frac{3}{2} \times \frac{1}{\left(1 + \frac{z^2}{a^2}\right)^{3/2}}$$

$(p = \frac{\text{wheel load}}{\text{contact area}})$ $p \rightarrow$ ^{tyre} ~~dist~~ pressure
 $\Rightarrow p \rightarrow$ wheel load

$$\Delta = \frac{P}{\pi a^2 \times E} \times a \times \frac{3}{2} \times \frac{a}{\left(a^2 + z^2\right)^{3/2}}$$

$$\therefore \left[z = \sqrt{\left(\frac{3P}{2\pi E \Delta}\right)^2 - a^2} \right] \leftarrow \text{Boussinesq's displacement equation.}$$

Drawbacks

- ↳ soils are not perfectly elastic and homogeneous
- ↳

$$p = \frac{P}{\pi a^2}$$

Problem

Calculate the vertical deflection at the surface of a flexible pavement due to a wheel load of 30kN and a tyre pressure of 0.75 MN/m². Take $E_{\text{pavement}} = E_{\text{subgrade}} = 15 \text{ MN/m}^2$

→ Solution,

- wheel load (P) = 30kN
- tyre pressure (p) = 0.75 MN/m²
- E = 15 MN/m²

$$\Delta_{\text{surf}} = ?$$

$$\Delta_{\text{surf}} = \frac{1.5pa}{E} = \frac{1.5 \times 0.75 \times 1000 \times 0.113}{15 \times 10^3} = 8.47 \text{ mm}$$

$$\text{contact radius } a = \sqrt{\frac{P}{\pi p}} = \sqrt{\frac{30}{\pi \times 0.75 \times 1000}} = 0.113 \text{ m}$$

$$(p = p \times \pi a^2)$$

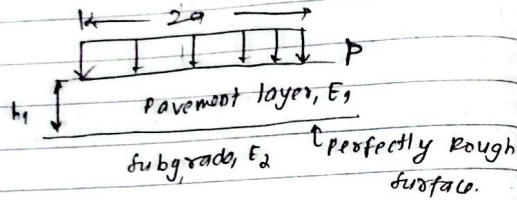
~~As 2B~~

(B) Semi-empirical Method

• Boussinesq's Theory

↳ By Donald M. Boussinesq, 1945

↳ stress and strain in two layered system (a pavement layer and a subgrade layer)



Assumptions:

↳ For large depth Boussinesq & Bousinesq's gives same depth (interface might differ)

↳ Interface: perfectly rough ($f=1$)
↓
stress distribution uniform
↳ coefficient of friction.

↳ Soil elastic, homogenous, isotropic, semi-infinite

↳ surface layer is free of shearing and normal stresses outside the loading area.

• Deflection at the surface (Δ)

For flexible circular plate:

$$\Delta = \frac{1.5pa}{E_2} F_w$$

For rigid circular plate

$$\Delta =$$

Displacement factor (F_w)

Depends. ↳ thickness (top layer) ↑ → F_w ↓
↳ strength ratio ($\frac{E_1}{E_2}$)

WASHO → Western Association of State Highway Officials
AASHO

Burnister's Theory

(3) Plate bearing tests were conducted with a 75cm dia plate on soil subgrade and a granular base. The stress was 0.02 MN/m^2 when the deflection on the subgrade soil was 0.25cm. The same plate yielded 0.25cm deflection on the base course of 15cm under a stress of 0.05 MN/m^2 . Design the pavement for an allowable deflection of 0.5 cm under a wheel load of 40kN and tire pressure of 0.05 MN/m^2 .

→ Plate bearing test:

Diameter of plate = 75cm, $a = 37.5 \text{ cm}$.

• On subgrade:

Deflection (Δ) = 0.25cm

Stress (p) = 0.02 MN/m^2

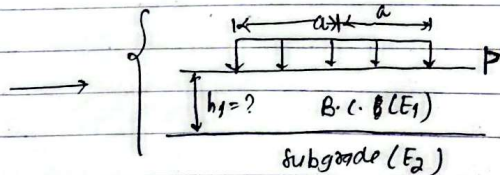
• On base course:

Thickness of b.c. (h) = 15cm

Def. (Δ) = 0.25cm

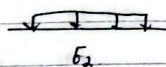
Stress (p) = 0.05 MN/m^2

Design:



on sub-grade:

$$\Delta = \frac{1.18 p a}{E_2} \quad (\text{on single layer rigid pavement})$$

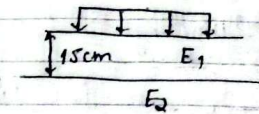


$$\text{or } 0.0025 = \frac{1.18 \times 0.02 \times 10^6 \times 0.375}{E_2}$$

$$\text{or } [E_2 = 3.54 \text{ MN/m}^2]$$

on base course

$$\Delta = \frac{1.18 p a}{E_2} \times \left(\frac{F_w}{E_2} \right) \quad \text{two layered system}$$



$$0.0025 = \frac{1.18 \times 0.05 \times 10^6 \times 0.375}{3.54 \times 10^6} \times F_w$$

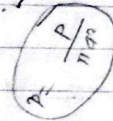
$$\Rightarrow [F_w = 0.4]$$

$$\text{For } F_w = 0.4, \quad \frac{h}{a} = \frac{15}{37.5} = 0.4$$

from chart, $\frac{E_1}{E_2} = 200$ [$F_w = 0.4$, $0.4a$]

$$[E_1 = 200 \times 3.54 = 708 \text{ MN/m}^2]$$

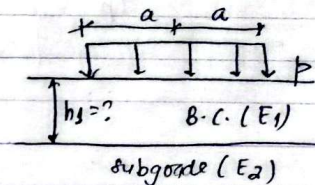
Thickness of top layer



Design:

$$\Delta_{\text{limiting}} = 0.5 \text{ cm}$$

$$\Delta_{\text{limit}} = \frac{1.18 p a}{E_2} \times (F_w)_{\text{limiting}}$$



$$\pi a^2 \times 40 = 0.5 \times 10^3 \quad \Rightarrow (\pi a^2 \times 0.5 \times 10^3 = 40) \quad b \times A = P$$

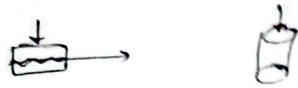
$$\Rightarrow [a = 0.16 \text{ m} = 16 \text{ cm}]$$

$$p = 0.5 \times 10^3 \text{ kN/m}^2$$

$$E_2 = 3.54 \times 10^3 \text{ kN/m}^2$$

$$\Delta_{\text{limit}} = 0.005 = \frac{1.18 \times 0.5 \times 10^3 \times 0.16}{3.54 \times 10^3} \times (F_w)_{\text{limiting}}$$

$$(F_w)_{\text{limiting}} = 0.1475 \approx 0.14 \text{ (round down)}$$



For, $(F_w)_{limiting} = 0.14, \frac{E_1}{E_2} = 200$

$h = 1.5a = 1.5 \times 16 = 24.8 \text{ cm}$

$h = 1.5a = 1.5 \times 16 = 24 \text{ cm}$
(Give multiple of 5mm)

Triaxial Method:-

- ↳ developed by Kansas State Highway Department
- ↳ based on Boussinesq's displacement eqⁿ.

Design thickness Equation:

↳ Based on Boussinesq's.

$$T = \sqrt{\left(\frac{3P}{2\pi E_s \Delta}\right)^2 - a^2}$$

↳ Final design thickness equation:

$$T_p = \left\{ \sqrt{\left(\frac{3PXY}{2\pi E_s \Delta}\right)^2 - a^2} \right\} \left(\frac{E_s}{E_p}\right)^{1/3}$$

Triaxial Method

Problem

Calculate the thickness of subbase, base and surface course using triaxial method with following data.

Wheel load (P) = 4080 kg

$E_{subgrade} (E_s) = 9015 \text{ kg/cm}^2$

$E_{sub-base} (E_{sub}) = 2701 \text{ kg/cm}^2$

$E_{base} (E_b) = 5401 \text{ kg/cm}^2$

$E_{surface} (E_{surf}) = 9000 \text{ kg/cm}^2$

Tire pressure (P) = 619 / cm²

Total traffic = 5000 vpd

Average annual rainfall = 80 cm

Permissible deflection (Δ) = 2.5 mm

→ Solution:-

For ADT = 5000 vpd, $X = 9/6$

For rainfall = 80 cm, $Y = 0.8$

Contact radius (a) = $\sqrt{\frac{P}{\pi p}} = \sqrt{\frac{4080}{\pi \times 6}} = 14.71 \text{ cm}$

Thickness equation:

Taking $E_p = E_{surf} = 9000 \text{ kg/cm}^2$

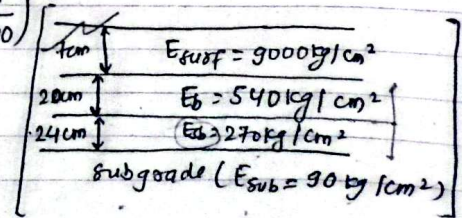
$$T_p = \sqrt{\left(\frac{3PXY}{2\pi E_s \Delta}\right)^2 - a^2} \times \left(\frac{E_{sub}}{E_{surf}}\right)^{1/3}$$

$$= \sqrt{\left(\frac{3 \times 4080 \times 9 \times 0.8}{2\pi \times 90 \times 0.25}\right)^2 - 14.71^2} \times \left(\frac{90}{9000}\right)^{1/3}$$

= 22.16 cm

(full depth bitumen design)

But we put 7cm (usually > 5cm) asphalt in surface



taking thickness of surface layer (t_{surf}) = 7cm
 converting remaining (22.16-7)cm to equivalent base material.

$$T_b = 15.16 \text{ cm} \times \left(\frac{E_{surf}}{E_b} \right)^{1/3}$$

$$= (15.16) \times \left(\frac{9000}{540} \right)^{1/3}$$

$$= 38.72 \text{ cm}$$

taking thickness of base layer (t_b) = 22cm (> 7 cm)

converting remaining (38.7-22) cm to equivalent subbase material

$$T_{sb} = t_b = (38.7 - 22) \times \left(\frac{E_b}{E_{sb}} \right)^{1/3}$$

$\left. \begin{array}{l} \text{must be } > 22 \text{ cm} \\ \text{else need to} \\ \text{revise } t_b \\ \text{st. } t_b > 22 \text{ cm} \end{array} \right\}$

$$= (38.7 - 22) \times \left(\frac{540}{270} \right)^{1/3}$$

$$= 21.06 \text{ cm} \quad (< 22 \text{ cm i.e. } t_b)$$

Again, let, $t_b = 20 \text{ cm}$ (NOT OK)

$$T_{sb} = t_b = (38.7 - 20) \times \left(\frac{540}{270} \right)^{1/3}$$

$$= 23.56 \text{ cm} \quad (> 22 \text{ cm i.e. } t_b)$$

So okay

Take, $t_b = 24 \text{ cm}$ (multiple of 5mm)

Empirical Method

- Based on Soil Classification (Ground Index Method)
- Based on Arbitrary soil strength test (CBR Method: IRC: 37-1970, Road Note 29, Road Note 31)
- Based on Pavement Performance (AASHTO Method)

Group Index (GI)

↳ An arbitrary number used in AASHTO soil classification.

$$GI = 0.2a + 0.005ac + 0.01bd$$

GI: 0 to 20

0 → Excellent

0-1 → Good

2-4 → Fair

5-9 → Poor

10-20 → Very poor

$F = 75 \text{ kN/m}^2$ (✓)

$LL =$

$IP = LL - PL$

$a = F - 35 \quad (0 - 40)$

$b = F - 15 \quad (0 - 40)$

$c = LL - 40 \quad (0 - 20)$

$d = IP - 10 \quad (0 - 20)$

→ Higher GI ⇒ lower strength ⇒ greater thickness of sub-base required

→ The thickness of base & surface is varied according to the volume of commercial traffic expected

• Traffic categories

Light volume traffic	< 50	commercial traffic/day
Medium	50-300	
heavy	> 300	

GI Method

(9) A subgrade soil sample has following properties:
 Soil passing 75 micron sieve = 60% = % fine (F)

Liquid limit (LL) = 65%

Plastic limit = 35%

Design the pavement section by group index method for heavy traffic with over 400 commercial vehicles per day (cvpd)

→ Solⁿ:

% fine (F) = 60%

Liq. limit (LL) = 65%

Plas. limit (PL) = 35%

Plasticity Index (Ip) = 65 - 35 = 30%

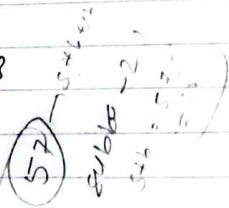
Traffic = 400 cvpd (>300 ⇒ heavy traffic)

$a = 60 - 35 = 25$

$b = 65 - 15 = 40$ } as b: ^{range} 0-40

$c = 60 - 40 = 20$

$d = 30 - 10 = 20$



$GI = 0.2a + 0.005ac + 0.01bd$

$= 0.2 \times 25 + 0.005 \times 25 \times 20 + 0.01 \times 40 \times 20$

$= 15.5 \approx 16$ (round up → as with 16 GI → thickness) (low strength) (reference)

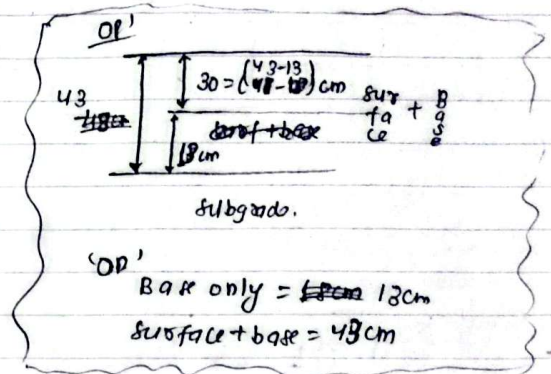
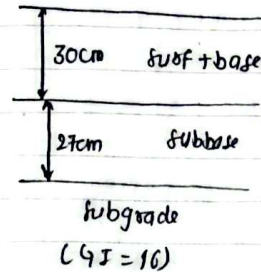
Thickness design:

GI = 16, Traffic = heavy.

Thickness of sub-base = 27cm (selected material subbase only)

Thickness of surf + base + subbase = 57cm

Thickness of surface + base = (57 - 27) = 30cm



□ CBR Method

↳ California Bearing Ratio of subgrade soil

(IRC Recommended CBR)

Design a flexible pavement using CBR curves, given the following data:

Subgrade soil, CBR = 4%

Compacted sandy soil, CBR = 10%

Poorly graded gravel, CBR = 25%

Well-graded gravel, CBR = 90%

Minimum thickness of bituminous concrete surfacing = 5 cm

Number of heavy vehicle per day in Sept. 2021 = 1000

Design life = 10 yr.

Annual growth rate of traffic = 6%

If design period not given → take 1.5-2 yr

The road is proposed to be completed in September 2024.

→ Design traffic

Traffic at last count / base yr. traffic (P) = 1000 Cvpd

Design life (n) = 10 yr.

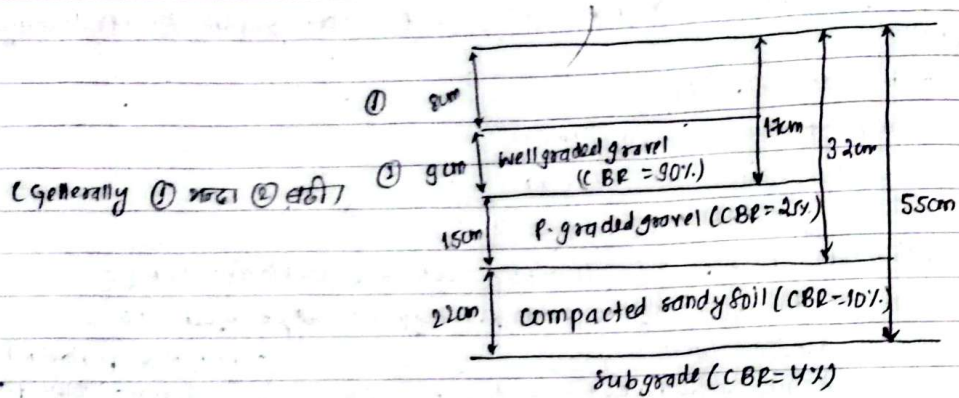
NO. of yr from last count to the completion of construction (y) = 3 yr

Expected traffic at the end of design life (A)

$$\begin{aligned} &= P(1+r)^{n+y} \\ &= 1000(1+0.06)^{10+3} \\ &= 2132.93 \\ &\approx 2133 \end{aligned}$$

(Design curve F as range: 1500-4500)

Bituminous surfacing.



- Drawbacks of IRC Recommended CBR
- ↳ Material specification of pavement not covered
 - ↳ Load repetition not covered (covered in Road Note 29)

Road Note 29 (RN-29) - Major change in design traffic consideration

→ A revised methodology based on CBR value by Transport and Road Research Laboratory (TRL) Britain
 - Introduced in 1960, revised in 1965, published a manual in 1970.

Major features.

- ↳ Use of cumulative of standard axles in the design life of pavement over number of commercial vehicles per day.
- ↳ Different design thickness charts:

- ① for sub-base (use CBR values) and
- ② for base and surfacing (with specified material and considering varying cumulative number of standard axles) → enable planning of stage construction

[Full scale test → Real test]

[↳ based on axle load consideration]

[Last stage construction]. } overlay construction later for extra years if design traffic ↑

Design steps

① Estimate cumulative number of standard axles:

(a) Determine cvpd per lane (slow lane) from traffic survey and convert it to 80kN equivalent single axle load (ESAL) to find the present base year traffic in number of axles per day. (Lane 3000)

(b) Determine the expected number of axles per day on the day it is opened using a suitable growth rate.

axle load → equivalency factor (It has given ASTM 4th power formula)

Thickness design:

Total pavement thickness required to cover subgrade of CBR 4% for DT of F = 54cm (from curve)
 ↑
 Daily traffic

Total pavement thickness required to cover compacted sandy soil of CBR 10% for DT of F = 32cm

Actual pavement thickness of compact sandy soil
 = 54 - 32
 = 22cm

Total pavement thickness required to cover poorly graded gravel of CBR 25% for DT of F = 17cm

Actual pavement thickness of poorly graded gravel = 32 - 17
 = 15cm

Total pavement thickness req^d to cover well graded gravel of CBR 90% for DT of F = 8cm

Actual pavement thickness of well graded gravel = 17cm - 8cm
 = 9cm

CBR test] → 12.5mm - 20mm
 ↳ sub-base, base to for 50%

① Determine number of axle loads per day for each year during the design life. The number of axle per day multiplied by 365 for each year of life is supposed to give the cumulative number of axle over the design life.

$$S = \frac{1 \times \{1 - (1+r)^n\}}{(1-r)} = \left\{ \frac{(1+r)^n - 1}{r} \right\}$$

$$\left\{ N = \frac{365A \{ (1+r)^n - 1 \}}{r} \right\} \quad \text{80\% वातावरणको No. of axle.}$$

Design traffic:

Present or base yr traffic = P esa/day
 (esa/day)
 (equivalent standard axle/day)

Expected traffic at the end of construction period
 (A) = P(1+r)^y esa/day

y → NO. of construction years

(वास्तविक एउटा वा traffic जस्ता जस्ता)

Traffic:

opening yr = 365 * P
 1st yr = 365 * A (1+r)
 2nd yr = 365 * A (1+r)(1+r)

nth yr = 365 * A (1+r)ⁿ

n = design period

cumulative no. of std. axle over the design life in design lane (N) = 365A { 1 + (1+r) + ... + (1+r)ⁿ }

$$S = \frac{365A \{ 1 - (1+r)^n \}}{1-r}$$

② Determine thickness of sub-base based on on the cumulative number

- DT → subgrade CBR → sub-base thickness
- (MSA) & (30%) → subgrade of subbase वातावरणको (no need to give subbase). } 30% or more है वातावरणको सबबेस होइ वा (subgrade) वातावरणको
- Min. req. of subgrade है वातावरणको → no need to give subbase
- > 0.5MSA & CBR < 30% → 150mm
- < 0.5MSA & CBR < 20% → 80mm
- < 0.5MSA & CBR < 2% → (CBR_{2%} thickness) + 150mm.

PN 29 Graph

③ Determine thickness of base course and surfacing using

DT \rightarrow CBR acc. to DT \rightarrow thickness of layer

EN-29

9) A double lane Highway is to be constructed for the present traffic load of 2200 cprd. The estimated rate of growth of traffic is 7% and the period of construction is 2 years. The highway is to be designed for a life time of 20 years after construction and CBR value of subgrade is 5%. Design the flexible pavement as per Road note 29. Adopt number of standard axle per commercial vehicle = 1.0.

\rightarrow Design Traffic:

$$\begin{aligned} \text{Present or base year traffic (P) in design lane} &= \frac{2200}{2} \left[\begin{array}{l} \text{Assuming direction} \\ \text{distribution 50/50} \\ \text{percent} \end{array} \right] \\ &= 1100 \text{ cprd/day} \\ &\xrightarrow{\text{correcting factor}} \frac{1100 \times 0.07}{100} \\ &= 1188 \text{ era/day} \end{aligned}$$

Expected traffic at the end of construction period (A)
(or before the road opens to traffic)

$$\begin{aligned} A &= P(1+r)^y \text{ era/day} \\ &= 1188 (1+0.07)^2 \\ &= 1360.14 \text{ era/day} \end{aligned}$$

Cumulative no. of std. axle over the design life in design lane (N)

$$\begin{aligned} N &= \frac{365 A \{ (1+r)^n - 1 \}}{r} \text{ era} \\ &= \frac{365 \times 1360.14 \{ (1+0.07)^{20} - 1 \}}{0.07} \end{aligned}$$

$$= 20.4 \text{ msa} \quad \left\{ n=20 \right\}$$

Thickness design:

Subgrade CBR = 5%

Design traffic = 20.4 msa.

Thickness of rubber = 280mm

Alt. I:
Alternative

Dense Macadam
Thickness of base (DM) = 180mm
" " surface = 100mm

Alt. II

Thickness of base (rolled asp.) = 150mm
" " surface = 100mm

Alt. III: (chart)

Thickness of base (lean concrete) = 210mm
Thickness of surface = 130mm

{ * if heavy \rightarrow 30mm can be converted to composite base course
(चालक) 30mm में बिटुमन को मिलाकर

considered local condition

used in DPR

sub-tropical countries

Road Note 31 / Catalogue Method

\rightarrow Based on research conducted in countries throughout the world by Transport Research Laboratory UK. (TRL, UK)

\rightarrow First published in 1962, Overseas Road Note 31 (Fourth Edition) in 1993

- o cater traffic up to 30 million ESAL
- o consider variability in material properties, uncertainty in traffic and effect of climate and high axle load.

Design steps:

① Estimating amt. of traffic and cum. number of equivalent standard axles that will use the road over the selected design life;

o Only the total number and the axle loading of the heavy vehicles (unladen wt. of 3000Kg or more) needs be considered
 \rightarrow load को मात्र (self wt. excluded)

SL 16

OD \rightarrow origin Destination survey study.

Classify count \rightarrow min. 3 days
Locations, 7 days

(Dissection highway का 2 अंश के design lane परमाणु)

RN31

Q. RN31) Catalogue Method

In a certain section of single lane road, it is intended to construct the road pavement. The traffic survey shows that the road carries present AADT of 132 cv/day. The annual growth of traffic is 7%. The pavement is to be designed for 10 years period and expected completion period is 2 years from the last date of traffic count. (CBR test values of subgrade soil)

Penetration mm	Load kg	Penetration mm	Load kg
0.0	0.0	3.0	56.5
0.5	5.0	4.0	67.5
1.0	16.2	5	75.2
1.5	28.1	7.5	89.0
2.0	40.0	10.0	99.5
2.5	48.5	12.5	106.5

Adopt equivalency factor for each commercial vehicle in 80KN single axle load = 1. Design pavement section as per RN31 Guideline.

→ 1. Design traffic:
 Present or base yr. traffic (P) = 132 × 1 ea/day
 (single lane) ← *equivalency factor*
 = 132 esa/day single lane.

Expected traffic at the end of construction period (A)

$$A = P(1+r)^N$$

$$= 132(1+0.07)^{10}$$

$$= 151.13 \text{ esa/day}$$

Cumulative no. of std. axles over the design life in

$$\text{design lane (N)} = \frac{365 \times A \times [(1+r)^n - 1]}{r}$$

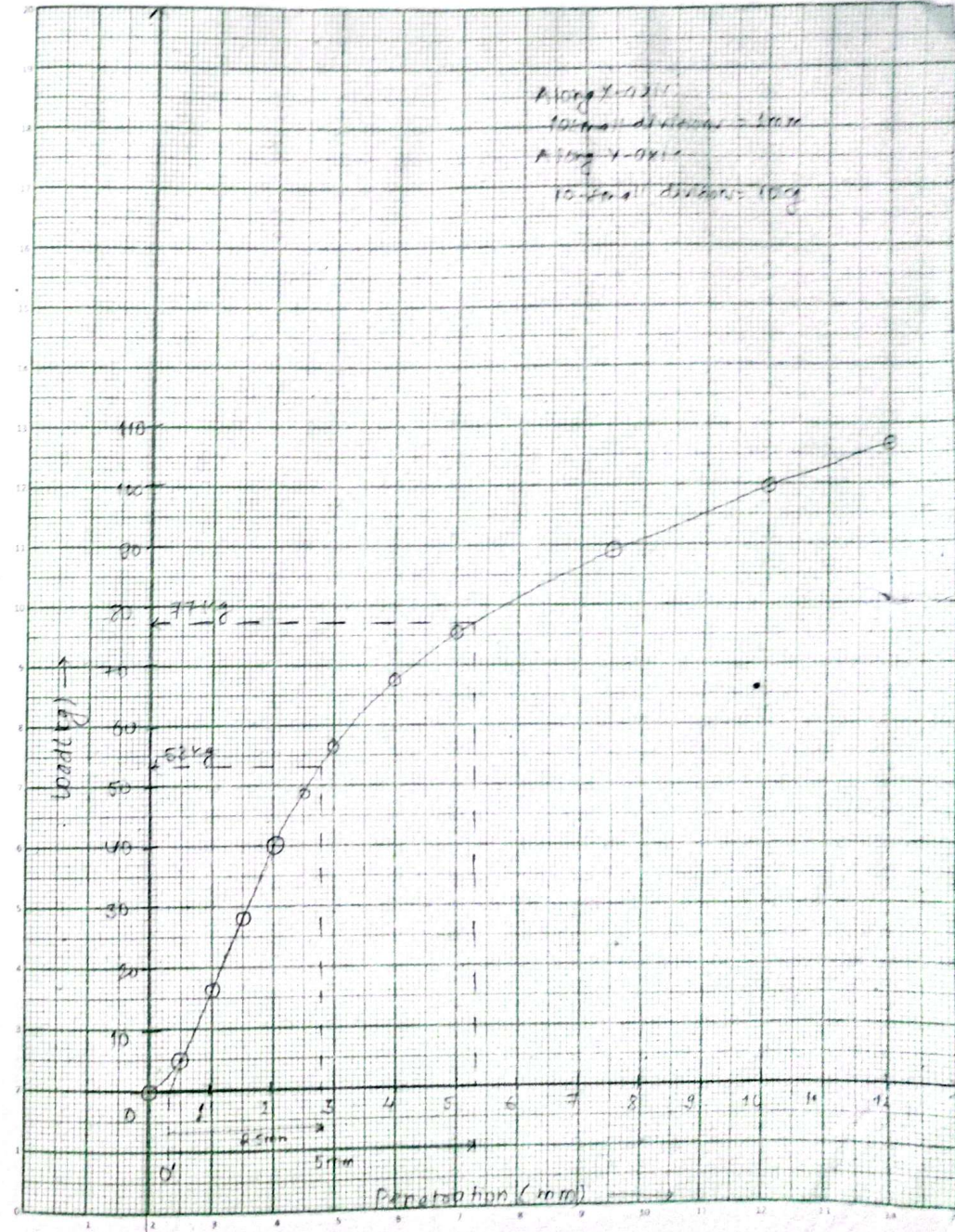
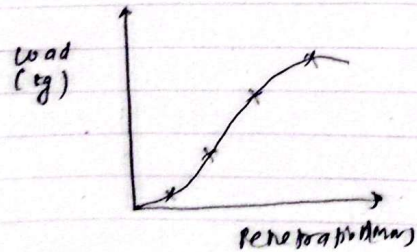
$$= \frac{365 \times 151.13 \times [(1+0.07)^{10} - 1]}{0.07}$$

$$= 0.76 \text{ msa}$$

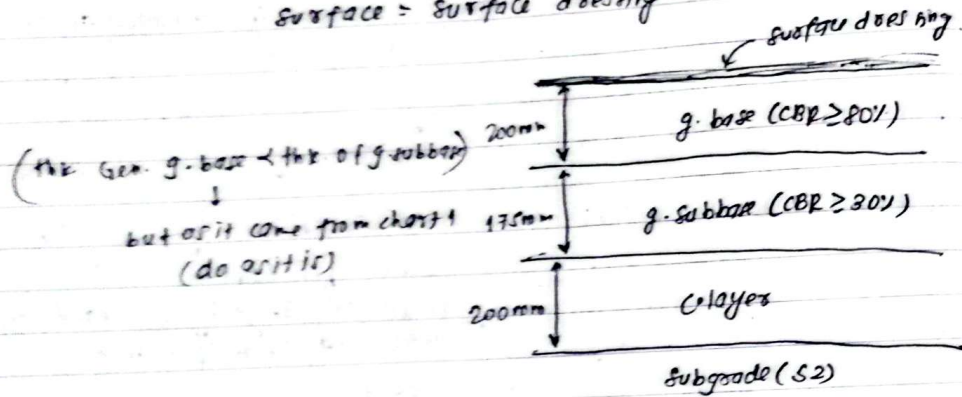
(million standard axles)

2. Design CBR

Load at 2.5mm penetration = 50kg
 Load at 5mm penetration = 77kg



Thickness of capping layer = 200 mm (T3-S2)
 Thickness of granular subbase = 175 mm (T3-S2) } chart 1.
 Thickness of granular base = 200 mm (T3-S2)
 surface = surface dressing



AASHTO Method

↳ US (AASHTO 1993)

↳ empirical method based on field performance data measured at AASHTO road test.

↳ design parameter

• Serviceability

$$PSI = 5.03 - 1.91 \log(1 + SV) - 1.38 RD^2 - 0.01 AC + P$$

where,

SV = slope variance (measure of roughness)

RD = Average rut depth (inches)

C+P = Area of cracking and patching per 1000 ft²

PSI	Objective rating
4-5	Very good
3-4	Good
2-3	Fair
1-2	Poor
0-1	Very Poor

Design equation

$$\log_{10}(W_{18}) = Z_{Rf} + 9.36 \log_{10}(SN+1) - 0.20 + \frac{\log_{10} \left(\frac{\Delta PSI}{4.2-1.5} \right) + 2.32 \log_{10} MR}{0.4 + \frac{1.62}{(SN+1)^{5.19}}} - 8.07$$

where,

W₁₈ = Number of 18 kips ESALs.

Z_R = standard normal deviate.

Z_p & S_0 → Reliability parameter.

S_0 = standard deviation
 ΔPSI = Allowable serviceability loss at end of design life.

M_R = Resilient modulus (psi) of road base

SN = structural number.

Q) Design a pavement for a rural highway using AASHTO flexible design procedure. The expected traffic design ESAL is 13×10^6 . The pavement structure is to consist of asphalt concrete with an elastic modulus of 400,000 psi, a granular base with an elastic modulus of 26,000 psi and a granular subbase with an elastic modulus of 12,000 psi. The drainage conditions of base and sub-base are fair. It is estimated that the pavement will be saturated about 15% of the time. Assume that a reliability level of about 90% is required and that the initial serviceability index is 4.2 and final serviceability index is 2.5.

AASHTO Method

1) $W_{18} = 13 \text{ msa} = 13 \times 10^6$

2) Reliability, $R = 90\%$

overall std. dev. $S_0 = 0.45$ (assume)

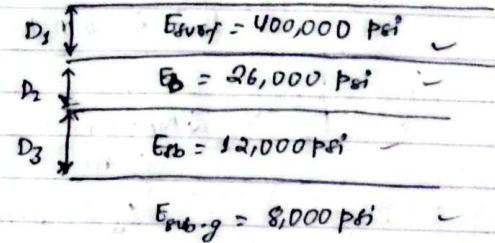
std. normal deviate $Z_p = -1.28$

3) Allowable serviceability loss,

$$(\Delta PSI) = P_0 - P_t$$

$$= 4.2 - 2.5$$

$$= 1.7$$



4) M_R depends on SN:

SN_1 (surface), $M_R = 26,000 \text{ psi}$ (base)

SN_2 (surface + base), $M_R = 12,000 \text{ psi}$ (subbase)

SN_3 (surface + base + subbase), $M_R = 8000 \text{ psi}$

5) $[SN_1 = 3.3$

$SN_2 = 4.4$

$SN_3 = 5.04]$ calculator

chart (negat)

$[SN_1 = 3.3$

$SN_2 = 4.3$

$SN_3 = 5.0]$

6) Layer's structural coefficients:

$\alpha_1 = 0.42$ (chart) → for surface, $E = 400,000 \text{ psi}$

$\alpha_2 = 0.249(\log E_b) - 0.977 = 0.122$

$\alpha_3 = 0.227(\log E_b) - 0.839 = 0.087$

7) Drainage coeffs:

$m_2 = 0.9$

$m_3 = 0.9$

same drainage condition for both

(fair & 15% moisture level)

⑧ . $SN_1 \leq \alpha_1 D_1$ (all in inches).

$$D_1 \geq \frac{SN_1}{\alpha_1} \geq \frac{3.3}{0.42}$$

$$D_1 \geq 7.86 \text{ inch} \approx 7.9 \text{ inch (round up)}$$

$$D_2 \geq \frac{\delta N_2 - \alpha_1 D_1}{\alpha_2 m_2} \geq \frac{4.3 - 0.42 * 7.86}{0.122 * 0.9}$$

$$D_2 \geq 9.108 \text{ inch}$$

$$D_3 \geq \frac{SN_3 - \alpha_1 D_1 - \alpha_2 m_2 D_2}{\alpha_3 m_3}$$

$$\geq \frac{5 - 0.42 * 7.86 - 0.122 * 0.9 * 9.108}{0.087 * 0.9}$$

$$\geq 8.95 \text{ inch}$$

Minimum check

$$D_1 = 7.9 \text{ inch} > 4 \text{ inch O.K.}$$

$$D_2 = 9 \text{ in} > 6 \text{ in O.K.}$$

$$D_3 = 9 \text{ in}$$

Mechanistic - Empirical Methods

→ consider mechanics of materials together with observed performance.

→ Pavement configuration, structural model (stress/strain), (distress modal/failure criteria)

Asphalt Institute Method

↳ earliest mechanistic-empirical method.

↳ A series of thickness design manual (1981 & later editions)

↳ Based on theories and empirical observations.

↳ Can be used to design various combination of asphalt.

• Design principle:

↳ pavement regarded as a multi-layered elastic system.

Asphalt concrete surface

Asphalt concrete or
emulsified asphalt
base

subgrade

Full depth asphalt
pavement

Asphalt concrete surface

Asphalt concrete or emulsified
asphalt base

Granular base

subgrade

Pavement with granular
base

• Failure criteria

◦ Fatigue cracking:

$$N_f = 1.365 (E_t)^{-0.3291} (E)^{-0.284}$$

where,

$$N_f =$$

◦ Rutting failure

$$N_d = 1.365 \times 10^{-9} (E_c)^{-4.477}$$

• Design subgrade resilient Modulus (M_R):

→ recommends triaxial tests for determining M_R , otherwise can

• Design steps

1. Determine design traffic (cumulative ESAL)
2. Determine design subgrade M_R .
3. Determine thickness of full depth asphalt concrete using design corresponding chart. Assume 50mm surface course and calculate the thickness of base course.
4. Determine thk. of emulsified asphalt base and untreated aggregate base using

Q) Design a pavement for a certain length of existing single lane carriageway with the following data. CBR results of subgrade soil obtained from seven locations in the stretch are given in the table:

- a) Current traffic of 80KN equivalent single axle load = 0.26×10^3 EA/day
- b) Design period = 10 yrs
- c) Construction period = 12 months from last traffic count
- d) Traffic growth rate = 8%
- e) Elastic modulus of asphalt concrete for surface course, $E_{ac} = 2500$ MPa.
- f) " " " emulsified stabilized base, $E_b = 1200$ MPa.
- g) " " " granular sub base (CBR $\geq 30\%$), $E_b = 150$ MPa.
- h) Draw the X-section of final pavement layers considering the thickness of asphalt concrete on the surface course not less than 75mm.

SN	1						
Chainage	0+50	0+350	0+500	0+650	0+800	0+950	1+500
Tert. CBR	11	9	7	8	6.5	5	4
or sub base							

→ Soln:

Design traffic (N):

Current or base year traffic (P) = 0.26×10^3 ESAL/day

[lane distribution & directional distribution is 1 for single lane]

Expected traffic at the end of construction period
 $(A) = P(1+r)^y$ ($y = 18 \text{ months} = 1.5 \text{ yrs.}$)

$$= 0.48 \times (1+0.08)^{1.5}$$

$$= 0.49 \times 10^5 \text{ SA}$$

Cumulative no. of standard axle over the design life

in design lane $(N) = \frac{365 A [(1+r)^n - 1]}{r}$

$$= \frac{365 \times 0.49 \times 10^5 \times [(1+0.08)^{10} - 1]}{0.08}$$

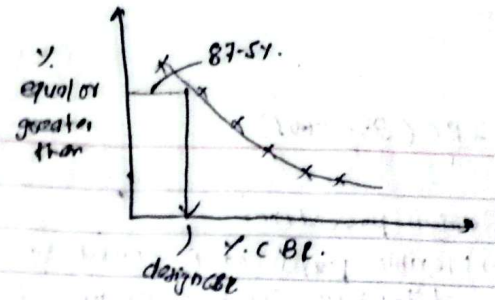
$$= 1.54 \text{ msa.}$$

② Design subgrade resilient modulus (M_R) = $10.3 \times \text{Design CBR}$

Design CBR = 87.5th percentile CBR ($N > 1 \text{ msa}$) = 4.9%

S.N.	(dec. order) % CBR	No. of reading equal or greater than	% Reading equal or greater than
1	11	1	14.28
2	9	2	28.57
3	8	3	42.86
4	7	4	57.14
5	6.5	5	71.43
6	5	6	85.71
7	4	7	100

Design $M_R = 10.3 \times \text{Design CBR}$
 $= 50.47 \text{ MPa}$



(3) Thickness design

Thickness of full depth asphalt concrete required for
 $(N = 1.54 \text{ msa}) ; M_R = 50.47 \text{ MPa} = 225 \text{ mm.}$

(Form chart A-1)

(50.47 MPa & 1.54 msa)

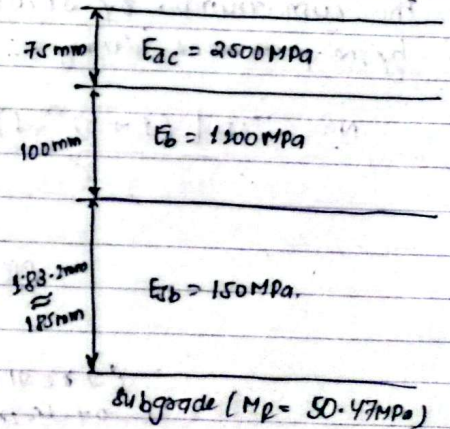
→ Taking thickness of asphalt concrete surface layer = 75 mm & (cm)

→ Converting remaining (225-75) mm to equivalent emulsified stabilized base $T_b =$

($\text{thb} > 6 \times 26$)

$$T_b = (225 - 75) \left(\frac{2500}{1200} \right)^{1/3}$$

$$= 191.58 \text{ mm.}$$



Taking thickness of emulsified stabilized base = 100 mm &

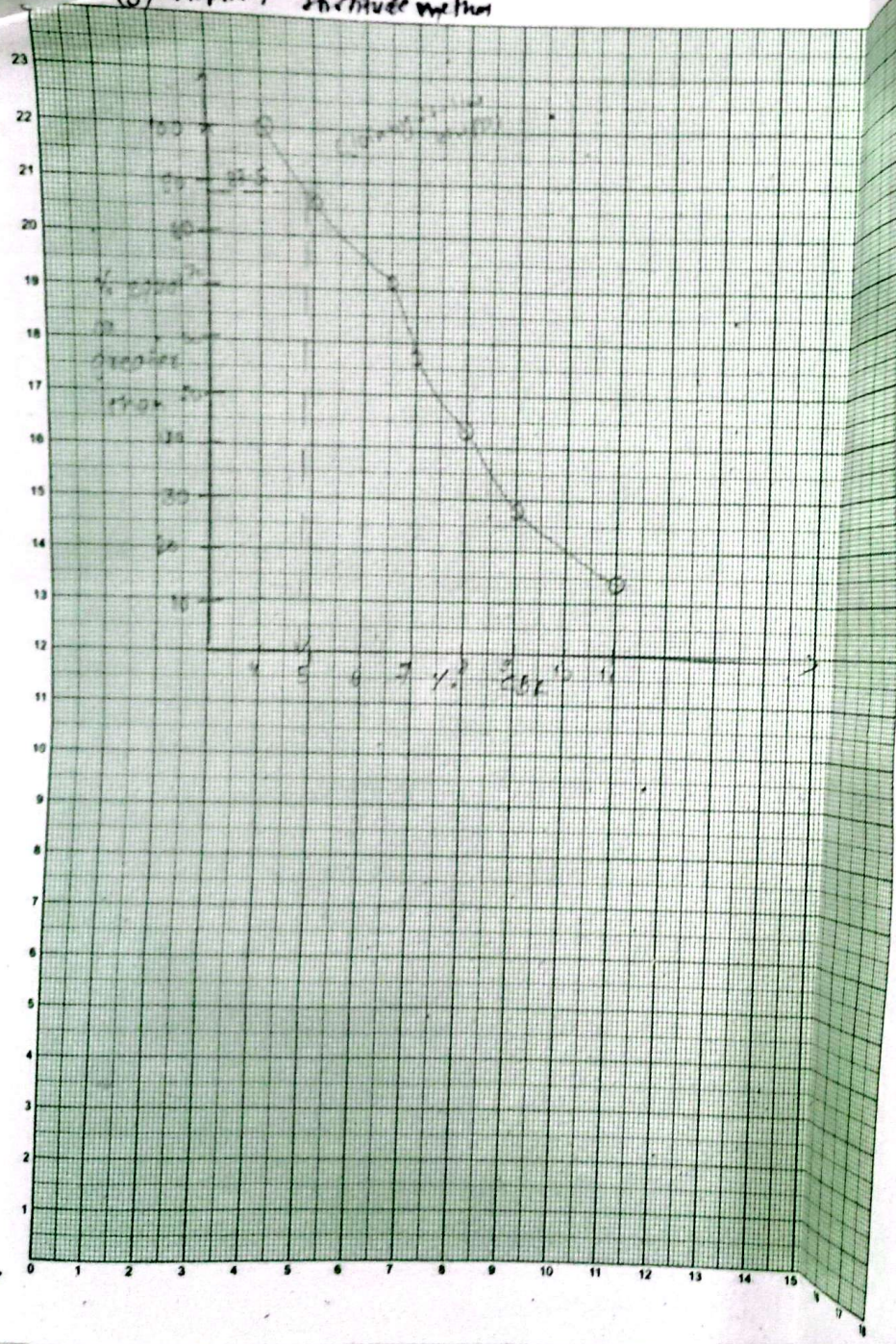
→ Converting remaining (191.6 - 100) mm to emulsified granular subbase

$$t_{sb} = (191.6 - 100) \times \left(\frac{1200}{150} \right)^{1/3}$$

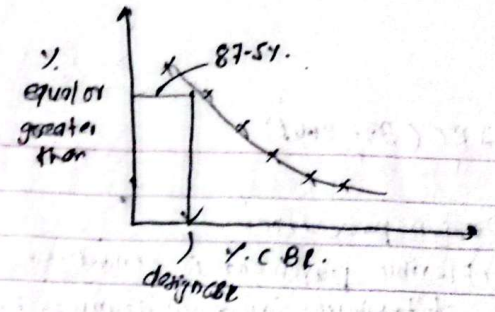
$$= 183.2 \text{ mm.}$$

$$\approx 185 \text{ mm.}$$

(9) Asphalt In-situ method



Design $M_R = 10.3 \times \text{Design CER}$
 $= 50.47 \text{ MPa}$



(3) Thickness design

Thickness of full depth asphalt concrete required for
 $(N = 1.54 \text{ msa}) ; M_R = 50.47 \text{ MPa} = 225 \text{ mm}$.
 (From chart A-1)

(50.47 MPa & 1.54 msa)

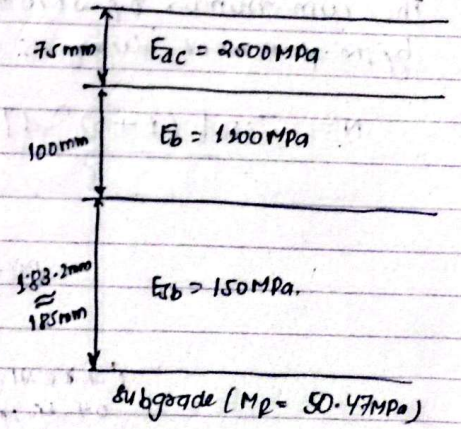
→ Taking thickness of asphalt concrete surface layer = 75 mm & (cm)

→ Converting remaining (225-75) mm to equivalent emulsified stabilized base $T_b =$

$T_b = \left(\frac{E_2}{E_1} \right)^{1/3}$

$T_b = (225-75) \left(\frac{2500}{12500} \right)^{1/3}$
 $= 191.58 \text{ mm}$

(note: $a_c > b \times 2.6$)



→ Taking thickness of emulsified stabilized base = 100 mm &

→ Converting remaining (191.6-100) mm to emulsified granular subbase

$t_{rb} = (191.6-100) \times \left(\frac{1200}{150} \right)^{1/3}$
 $= 183.2 \text{ mm}$

≈ 185 mm

IRC (37-2001)

• Design procedure:

- Flexible pavement is considered to comprise of 3 layers: bituminous surface, granular base and subbase course
- Analytical approach based on multiple layer elastic theory
- critical stresses and strains are computed from software FPAVE which uses:
 - Fatigue and rutting failure criteria were considered
 - Simple design charts and catalogue

• Design traffic:

The cum. number of standard axles (N) to be carried by the pavement during the design life in design lane.

$$N = \frac{365 [(1+r)^n - 1]}{r} \times A \times D \times F$$

lane
Distribution factor (LDF)

(A real estimate of distribution of commercial traffic by direction and by lane)

remains LDF values.

Problem 1

9. Design the flexible pavement for construction of a new road with the following data.

- 2-lane single carriageway is to be designed in plain area.
- Initial traffic in the year of completion = 310 ~~cpd~~ (sum of both directions)
- Traffic growth rate = 7%
- Design life = 15 yrs.
- Design CBR of subgrade soil = 5.0%

→ Solⁿ:

1. Design traffic:

Initial traffic in the year of completion of construction

$$(A) = 310 \text{ cpd}$$

$$(r) = 7\%$$

$$(n) = 15 \text{ years}$$

$$\checkmark \text{ VDF } (F) = 3.5 \text{ (from table)}$$

$$\text{LDF } (D) = 0.75 \text{ of both direction.}$$

$$N = \frac{365 A [(1+r)^n - 1]}{r} D \times F$$

$$= 7.46 \text{ msa}$$

2. Design subgrade CBR = 5%.

3. Thickness design:

Total thickness of pav. required = 620mm

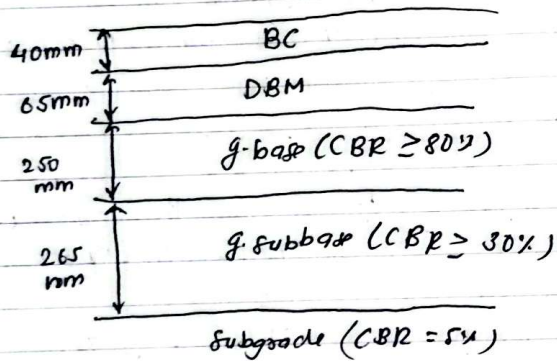
(Interpolate to multiple of 5)

Pg. 24

∴ [different material] ⇒ can't interpolate]

Total thickness of WC (surface) = 40 mm BC
 Total thickness of (Binding course surface) = 65 mm (DBM)
 " " " granular base = 250 mm
 " " " granular subbase = $\frac{620 - 40 - 65 - 250}{2}$

= 265 mm
 (∵ or = to interpolate value)



(IRC 37-2001)

- (Q) Design the flexible pavement for construction of a new road with the following data:
- 2-lane single carriageway is to be designed in plain area.
 - Initial traffic in the year of completion of construction = 310 cnpd (sum of both directions) with axle load distribution as given below:

Heavy truck (12t)	10%
Light truck (10t)	20%
Mini truck (8t)	40%
Large Bus (6t)	20%
Bus (5t)	10%

- Traffic growth rate = 7%
- Design life = 15 yrs
- Design CBR of subgrade soil = 5.0%

→ 1. Design traffic:

Initial traffic in the year of completion of construction
 (A) = 310 cnpd

$r = 7\%$

$n = 15 \text{ yrs}$

$LDF (D) = 0.75$

CV type	No. of CV	Axle load (KN)	Eq-factor	esd/day	No. of CV × Eq-factor
HT	31	120	5.0625	Eq-factor × 31 = 156.93	
LT	62	100	2.4414	151.36	
MT	124	80	1	124	
LB	62	60	0.8164	19.82	
B	31	50	0.1826	4.73	

Eq. factor

Assuming single axle dual wheels:

$$N = \frac{365 A_f (1+r)^n - 1}{r} \times D \times F$$

$$= \frac{365 \times 456.65 \times [(1+0.07)^{15} - 1] \times 0.75}{0.07}$$

$$= 314 \text{ m eq.}$$

2. Design subgrade CBR = 5%

3. Thickness design:

Total thickness of pavement required =

$$530 + \frac{580-530}{(5-3)} \times (3.14-3)$$

$$= 533.5 \approx 535 \text{ mm}$$

total thk. of WC (surf. face) = 20 (PC)
 " " " Bind. cover (surf. face) = 50 mm (BM)
 " " " g. base = 250 mm
 " " " g. sub-base = 535 - 50 - 250 = 235 mm
 (not taking 20 mm WC surf. face)
 (> 230 mm)
 OK

(Pg. 24) 20 mm or less still ok thickness still contribute sign

DOR (2021)

p. Design the flexible pavement for construction of new road with the following data for the flexible pavement design:

(a) 2-lane single carriageway is to be designed in plain area.
 (b) Initial traffic in the year of completion of construction = 310 crpd (sum of both directions as mentioned below)

- (i) Heavy truck (3 axle) = 30
- (ii) Heavy truck 2-axle = 70
- (iii) Mini truck = 120
- (iv) Large bus = 60
- (v) Bus = 30

- (c) Traffic growth rate = 7%
- (d) Design life = 15 yrs.
- (e) Design CBR of subgrade soil = 5%

→ Solⁿ:

1. Design traffic

Initial traffic in the year of completion of construction

(A) = 310 crpd

(r) = 7%

n = 15 yrs.

LDF (D) = 0.75 VDF * No. of CV

CV type	No. of CV	VDF	es/day
HT	30	6.5	195
LT	70	4.75	332.5
MT	120	1	120
LB	60	0.5	30
B	30	0.35	10.5

688 esd/day

Assuming single axle dual wheels

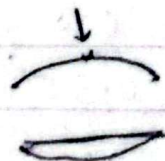
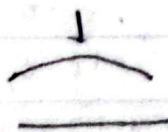
$$N = \frac{365 A \{ (1 + \delta)^n - 1 \}}{\delta} \cdot D \cdot F$$
$$= \frac{365 \times 688 \{ (1 + 0.07)^{15} - 1 \}}{0.07} \times 0.75$$
$$= 4.73 \text{ meq/day.}$$

2. Design CBR = 5%

3. Thickness design : $N = 5 \text{ meq, CBR} = 5\%$

Total thickness of pav. required = 490 mm (AC)

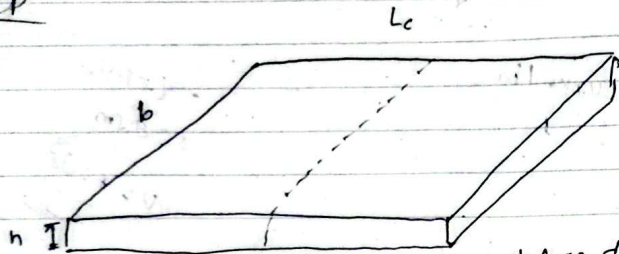
- i / " " WC (surface) = 40 mm
- ii " " Bind. course (surface) = 0 mm
- iii " " g. base = 250 mm
- iv " " g. subbase = 200 mm.



~~# Westg~~ # Westergaard's Theory.

Wheel load stress

JPCP



← F_f → frictional force due to concrete shrinkage or seasonal temperature change.

$$L_c = \frac{2 S_c \times 10^4}{W f} \quad (\text{for PCC pavement})$$

$$L_c = \frac{200 A_s \times S_c}{W b f h} \quad (\text{For RC pavement})$$

→ Frictional force developed = $W \times f \times \frac{L_c}{2} \times b \times h / 100$

↓
Coeff of friction.

→ Allowable tension in concrete = $S_c \times 10^4 \times b \times h / 100$

$$W \times f \times \frac{L_c}{2} \times b \times h / 100 = S_c \times 10^4 \times b \times h / 100$$

$$\left[L_c = \frac{2 S_c \times 10^4}{W f} \right]$$

For JPCP,

$$W \times f \times \frac{L_c}{2} \times b \times h / 100 = S_c \times A_s$$

$$\left[L_c = \frac{200 S_c \times A_s}{W f b h} \right]$$

Design of slab thickness

1. Width of slab (b_f) = 3.5m

$$2. \text{Length of slab } (l) = \frac{2 \times 0.8 \times 10^4}{24 \times 3.5}$$

$$= 44.5m < 4.5m \text{ (ok)}$$

3. Assume: $h = 20\text{cm}$

4. Radius of relative stiffness:

$$l = \left[\frac{(h^3)}{12(1-\mu^2)k} \right]^{1/4}$$

$$l = \left[\frac{2 \times 10^5 \times 20^3}{12(1-0.15^2)} \right]^{1/4}$$

$$l = 71.1\text{cm}$$

Warping stress of edge: $\frac{2m}{l} = \frac{4.45 \times 100}{71.1} = 6.26$

$$C_1 = 0.95$$

$$\frac{2y}{l} = \frac{3.5 \times 100}{71.1} = 4.92$$

$$C_2 = 0.698$$

At free 20cm thickness, $\approx 15^\circ$

$$\sigma_{te} = 24 \text{ kg/cm}^2$$

(from chart)

5. Remaining strength = $40 - \sigma_{te} = 40 - 24 = 16 \text{ kg/cm}^2$

6. Load stress at edge (σ_e) from chart:

$$\sigma_e = 27 \text{ kg/cm}^2$$

7. Factor of safety = $\frac{\text{Req. strength}}{\sigma_e} = \frac{16}{27} = 0.59$

3. Assume, $h = 25 \text{ cm}$
 4. $l = \left[\frac{Ebs^3}{12(1-\mu^2)k} \right]^{1/4} = 90.67 \text{ cm}$

Warping stress at edge:

$$\frac{\sigma_x}{l} = \frac{4.45 \times 100}{90.67} = 4.91$$

$$C_x = 0.695$$

$$\frac{\sigma_y}{l} = 3.86$$

$$C_y = 0.463$$

at for 25cm thickness = ~~16.3°C~~ 16.3°C
 (table)

$$\sigma_{te} \text{ (from chart)} = 17.5 \text{ kg/cm}^2$$

5. Remaining strength = $40 - 17.5 = 22.5 \text{ kg/cm}^2$

6. Load stress at edge (σ_p) from chart
 $\sigma_p = 17.5 \text{ kg/cm}^2$

7. Factor of safety = $\frac{40}{17.5} > 1$

Now, corner

(8) Corner stress:

$$\text{Warping stress at corner } (\sigma_{te}) = \frac{E \alpha t}{3(1-\mu)} \sqrt{\frac{a}{l}}$$

$$= \frac{15 \times 10^5 \times 10 \times 16.3}{3(1-0.25)} \sqrt{\frac{15}{90.67}}$$

$$= 7.75 \text{ kg/cm}^2$$

Load stress at corner (σ_c) = 20 kg/cm^2
 (chart)

$$\sigma_{te} + \sigma_c = 27.75 < 40 \text{ kg/cm}^2 \text{ ok}$$

9. $P = 950 \text{ cwpd}$

Assume

$$n = 20 \text{ years}$$

$$r = 7.5\%$$

$$A = P(1+r)^n$$

$$= 950(1+7.5\%)^{20}$$

$$= 4085.46$$

Adjusted thickness = $25 + 0$ (No correction required)
 $= 25 \text{ cm}$

$$L_d = 5d \sqrt{\frac{F_f(L_d + 1.5d)}{F_b(L_d + 8.8d)}}$$

$$P_s = 0.785d^2 F_s$$

Q9) Design spacing & dowel bars of expansion joint for a concrete pavement with following details:

Design wheel load = 5000 kg.

$$[\alpha = 10 \times 10^{-6} / ^\circ\text{C}]$$

Design load transfer = 40%

Slab thickness = 20 cm

Expansion joint width (s) = 2 cm

Maximum variation of temp^r b/w summer and winter = 35°

Permissible flexural stress in dowel bar (F_f) = 1400 kg/cm²

" shear " " " (F_s) = 1000 kg/cm²

" bearing " " " (F_b) = 100 kg/cm²

Modulus of subgrade reaction = 8 kg/cm³

→ Solⁿ:

$$\begin{aligned} \text{(i) Spacing of expansion joints} &= \frac{s'}{100 \times \alpha \times \Delta t} \\ &= \frac{\text{Joint width}/2}{100 \times \alpha \times \Delta t} \\ &= \frac{2 \text{ cm}}{100 \times 10 \times 10^{-6} / ^\circ\text{C} \times 35^\circ\text{C}} \\ &= 28.57 \text{ cm} < 140 \text{ cm (OK)} \end{aligned}$$

Design of Dowel Bar

01) Dowel bar:

Assume diameter of dowel bar (d) = 2 cm (assume)

∴ Length of embedment (L_d) for equal capacity in flexural & bearing

$$\frac{2d^3 F_f}{(L_d + 8.8d)} = \frac{L_d^2 d F_b}{12.5(L_d + 1.5d)}$$

$$\Rightarrow L_d = 5d \sqrt{\frac{F_f(L_d + 1.5d)}{F_b(L_d + 8.8d)}} \quad (s = 2 \text{ cm})$$

$$\text{or } L_d = 5 \times 0.02 \times \sqrt{\frac{1400(L_d + 1.5 \times 0.02)}{100(L_d + 8.8 \times 0.02)}}$$

$$\Rightarrow L_d = 33.3 \text{ m} \approx 31.3 \text{ cm}$$

$$L = L_d + s = 33.3 \text{ cm} \approx 35 \text{ cm}$$

$$\text{Act. } L_d = 35 - 2 = 33 \text{ cm}$$

2. Load transfer capacity of each dowel bar:

$$\begin{aligned} P_s &= 0.785d^2 F_s \\ &= 0.785 \times 2^2 \times 1000 \\ &= 3140 \text{ kg} \end{aligned}$$

Fail in flexure

$$P_f = \frac{2d^3 F_f}{(L_d + 8.8d)} = \frac{2 \times 2^3 \times 1400}{(33 + 8.8 \times 2)} = 242.7 \text{ kg/min}$$

$$P_b = \frac{L_d^2 d F_b}{12.5(L_d + 1.5d)} = \frac{33^2 \times 2 \times 100}{12.5(33 + 1.5 \times 2)} = 484 \text{ kg}$$

3. Required load transfer capacity of effective dowel system

$$= \max. \left(\frac{0.4P}{P_s}, \frac{0.4P}{P_f}, \frac{0.4P}{P_b} \right)$$

$$= \max. \left[\frac{0.4 \times 5100}{3140}, \frac{0.4 \times 5100}{442.6}, \frac{0.4 \times 5100}{484} \right]$$

$$= 4.61$$

(4) Assuming spacing of 20cm c/c

[15cm, 20cm, 25cm, 30cm]

Assume

Radius of relative stiffness (R)

$$R = \left[\frac{Eh^3}{12(1-\mu^2)K} \right]^{1/4}$$

E =

$\mu = 0.5$

$$R = 71.1 \text{ cm}$$

h = slab thickness

Length upto which dowel bars are effective = 1.8R

$$= 1.8 \times 71.1$$

$$= 127 \text{ cm}$$

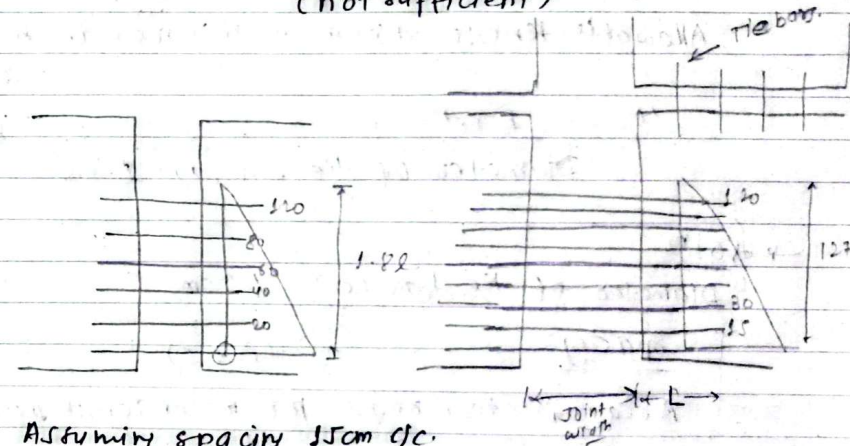
Load transfer capacity of eff. dowel bar system

$$= 1 + \frac{(127-40)}{127} + \frac{(127-40)}{127} +$$

$$+ \frac{(127-120)}{127}$$

$$= 3.69 < 4.61$$

(not sufficient)



Again, Assuming spacing 15cm c/c

Load t. capacity of eff. dowel bar system

$$= 4.75 > 4.61$$

OK

2cm ϕ , 35cm length, 15cm c/c

± Design of Tie Bar

A concrete pavement of 7.0m width has a thickness of 32cm and has a longitudinal joint. Design the dimension and spacing of the tie bars. Use the following data.

Unit wt. of concrete (w) = 2400 kg/cm³.

Allowable tensile stress in deformed tie bars (S_s) = 2000 kg/cm²

" bond " " " " (S_b) = 24.619/cm².

Diameter of tie bar (d) = 1.2cm.

→ Solⁿ

Diameter of tie bar (d) = 1.2cm

Spacing: ($f = 1.5$)

Area of steel reqd per meter length of long joint (A_s)

$$A_s \times S_s = \frac{W \times f \times l \times b \times h}{100}$$

$$\text{on } A_s \times 2000 = \frac{2400 \times 1.5 \times 1 \times \frac{7.0}{2} \times \frac{32}{100}}$$

$$[A_s = 2.01 \text{ cm}^2]$$

$$\text{Area of each tie bar } (a_s) = 1.13 \text{ cm}^2 = \frac{\pi \times d^2}{4}$$

$$\text{No of tie bars per m. length} = \frac{2.01}{1.13} \approx 2.$$

$$\text{Spacing} = \frac{100 \text{ cm}}{2} = 50 \text{ cm c/c}$$

Length (L_t):-

$$L_t = \frac{2 a_s S_s}{p \times S_b} = \frac{2 \times \frac{\pi d^2}{4} \times S_s}{\pi d \times S_b} = \frac{d}{2} \times \frac{S_s}{S_b}$$

$$= \frac{1.2}{2} \times \frac{2000}{24.61}$$

$$= \underline{81.39 \text{ cm}} \quad 48.78 \text{ cm.}$$

$$\text{Length} = L_t + (5 - p \text{ cm})$$

$$\approx \underline{49.5 \text{ cm}} \quad \underline{55 \text{ cm}}$$

(considering tolerance in placing)

Soil stabilization

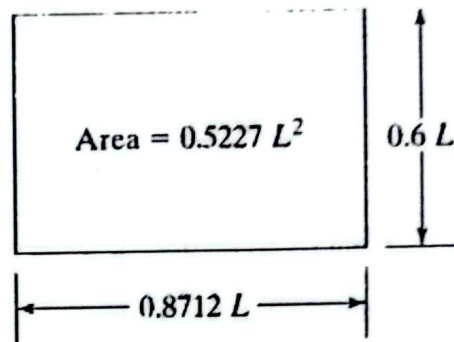
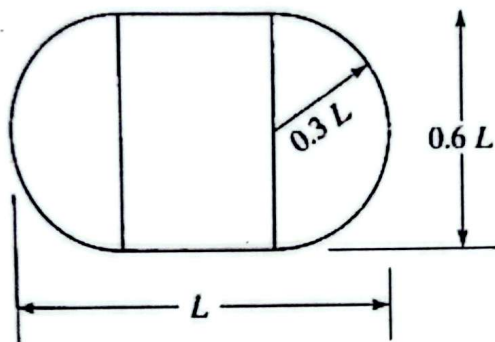
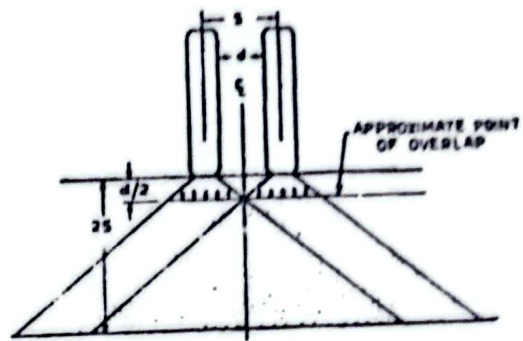
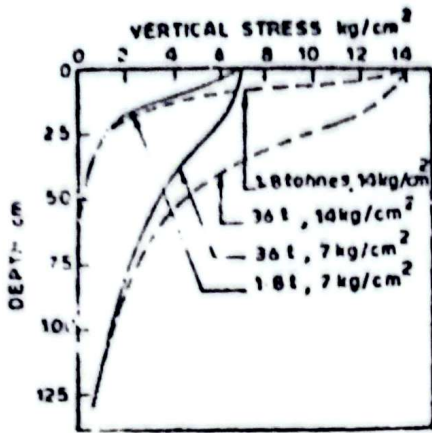
↳ Improving the strength of soil by proportioning and/or mixing with other materials & compaction.

✓ Increase Bearing capacity; increase shear strength; prevent cracks in soil; good drainage; less frost susceptibility

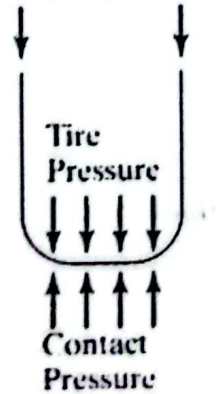
Basic principle:

- ↳ Evaluating properties of soil
- ↳ Deciding effective & economical method of soil stabilization
- ↳ Designing the mixes
- ↳ Compacting stabilized soil adequately

Mechanical ss	Soil-cement stab.	Soil-Lime	Soil-Bitumen
<p>→ Blending of two different materials to meet required strength, grading & plasticity criteria.</p> <p>→ Basic principle is proportioning & compaction</p> <p><u>Factors affecting:</u></p> <ul style="list-style-type: none"> ↳ Mechanical strength of aggregate ↳ Gradation ↳ Soil properties ↳ Presence of salt & water ↳ Compaction. <p><u>Desirable properties of soil:</u></p> <ul style="list-style-type: none"> ↳ Strength ↳ Incompressibility ↳ stability with variation in moisture content ↳ Good drainage. ↳ Less frost susceptibility ↳ Ease of compaction. <p><u>Equipment</u></p> <ul style="list-style-type: none"> ↳ Laboratory facilities for mix design ↳ rotator for compaction <p><u>Material selection</u></p> <ul style="list-style-type: none"> ↳ crushed stone <math>80\%</math> passing # 42 sieve & >85% passing # 40mm sieve. ↳ Max. size 60mm; CBR_{min} = 25% S_{max} = 95%. ↳ LL → 25% base & 35% surface ↳ PI → 6 base & (5-10) surface ↳ Fuller's formula. 	<p>→ Addⁿ of cem & water</p> <p>→ Stabilization is due to bond b/w cem. & soil particle & redⁿ in plasticity</p> <p>→ curing for 7 days</p> <p><u>Factors affecting</u></p> <ul style="list-style-type: none"> ↳ Nature of soil ↳ proportion of cem. ↳ compaction moisture content ↳ Dry density of mix (compact) ↳ Curing ↳ Additives. <p><u>Design of soil-cem mix</u></p> <ul style="list-style-type: none"> ↳ Based on fix off specimen cured for 7 days ↳ specimen: 5cm dia & 10cm ht with diff cem content compacted upto DMC ↳ Design cem-content corr. to 17-51% $1\text{cm}^2 \Rightarrow$ Medium traffic 35% $1\text{cm}^2 \Rightarrow$ High traffic. <p><u>Equipments</u></p> <ul style="list-style-type: none"> → Mix - rotator or manually → or mixing plant or cement truck mixer → compacting eqp. <p><u>Material selection</u></p> <ul style="list-style-type: none"> ↳ # 4.75 mm → > 50% ↳ # 75 μ → 50% ↳ LL > 40% ↳ PL → > 18% ↳ cem content: 5-14% by vol. <p><u>Field control</u></p> <ul style="list-style-type: none"> ↳ moisture content; ° of pulverization; cem content; fc; S_{dry}; surface regularity. 	<p>→ Addⁿ of lime</p> <p>→ More effective option for plastic clay.</p> <p>→ 4-8% by wt. is usually mixed on-site then compacted at suitable moisture content and cured for about 14 days.</p> <p><u>Factors affecting</u></p> <ul style="list-style-type: none"> ↳ similar or ber. etc. ↳ Lime content ↳ type of lime (quick lime, CaO, Hydrated lime) <p><u>Design of mix</u></p> <ul style="list-style-type: none"> ↳ Non standard method ↳ lime content is based on lime fixation limit or amount reqd to reduce PI or finellity value to desired level. <p><u>Equipments</u></p> <ul style="list-style-type: none"> → For spreading, pulverizing, mixing & compacting <p><u>Material selection</u></p> <ul style="list-style-type: none"> → lime of consistent quality. → Fresh water for compaction moisture control & curing 	<p>→ Modification of sub-standard locally available materials through addition of bitumen</p> <p>→ Bitumen emulsion is an effective option for strengthening non plastic sandy materials.</p> <p>→ normally 4-8% residual bitumen is usually mixed.</p> <p><u>Factors affecting</u></p> <ul style="list-style-type: none"> ↳ Bitumen content ↳ type of bitumen ↳ Additives (anti-stripping & reactive chemical additive) <p><u>Design of mix</u></p> <ul style="list-style-type: none"> ↳ No standard method ↳ specimen prepared with various bitumen contents and are tested for stability and water absorption. <p>→ <u>Equipment</u></p> <p><u>Material selection</u></p> <ul style="list-style-type: none"> → local sandy soil compatible with emulsion modification → slow setting emulsion → soil [# 4.75 → 90%, # 0.425 → 35 to 100%, # 0.075 → 10-50%, LL - 40%, PL - 18%] <p><u>Field control</u></p> <ul style="list-style-type: none"> → checking pulverization → moisture & bitumen content → S_{dry} after compaction

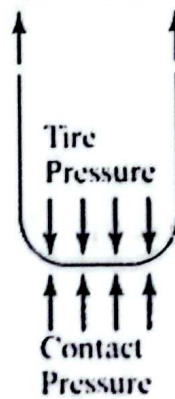


Wall of Tire
in Compression



(a) Low Pressure Tire

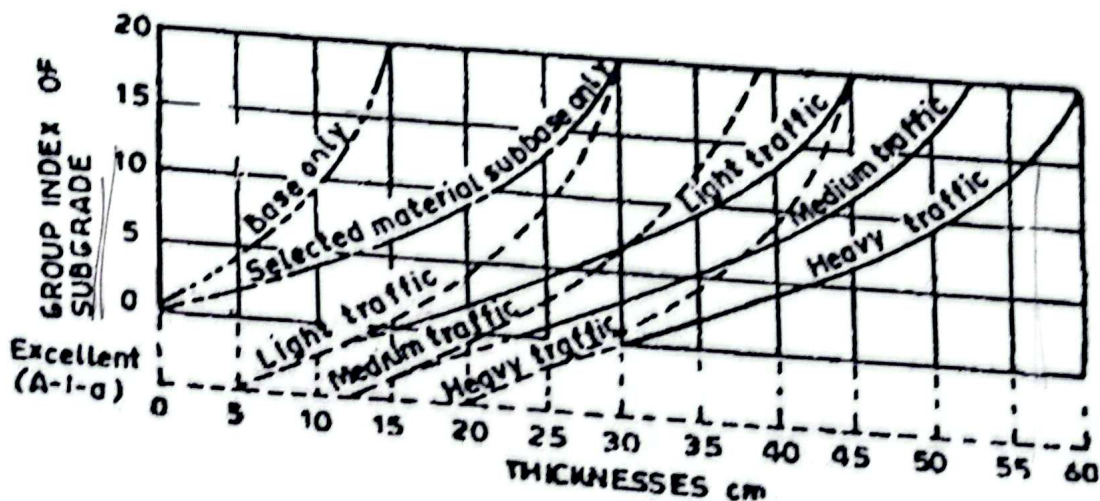
Wall of Tire
in Tension



(b) High Pressure Tire

GENERAL EVALUATION OF SUBGRADE	GROUP INDEX RANGE OF SUBGRADE	DAILY VOLUME OF COM. TRAFFIC			THICKNESS
		LIGHT (LESS THAN 50)	MEDIUM (50 TO 300)	HEAVY (MORE THAN 300)	
EXCELLENT (A-1-a)					30 cm
GOOD	0 - 1	15 cm	20.5 cm	30 cm	SURFACE AND BASE THICKNESS VARY WITH VOLUME OF TRUCK TRAFFIC 10 cm (min. not used generally) (surf + base)
FAIR	2 - 4	0 cm			
POOR	5 - 9	10 cm	10 cm	10 cm	SELECT SUB-BASE THICKNESS, VARY WITH SUBGRADE CHARACTERISTICS
VERY POOR	10 - 20	20 cm	20 cm	20 cm	

(a)



(b)

Group Index Method

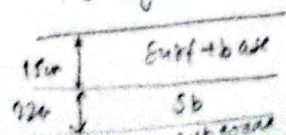
----- surface + base system
 _____ surface + base + subbase system

----- surface + base
 _____ subgrade

----- surface + base
 _____ subbase
 _____ subgrade

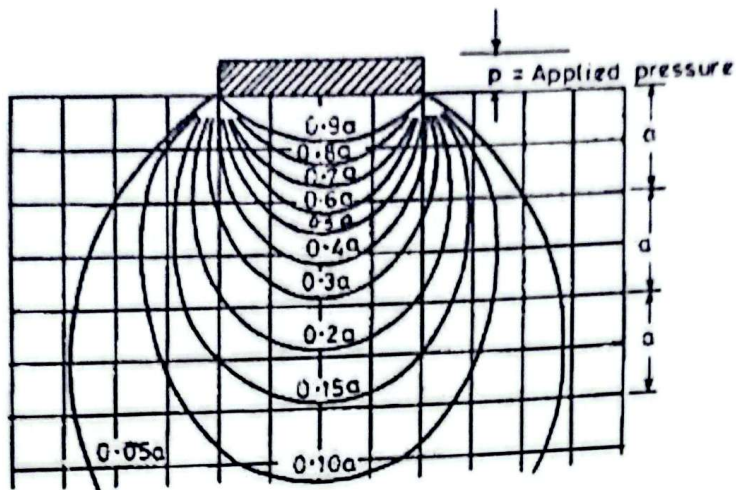
eg: (GI = 10)

Subbase = 22 cm
 Light traffic: Surf + base + Sb = 37 cm (→)
 Surf + base = 37 - 22 = 15 cm.
 (3 layer system)

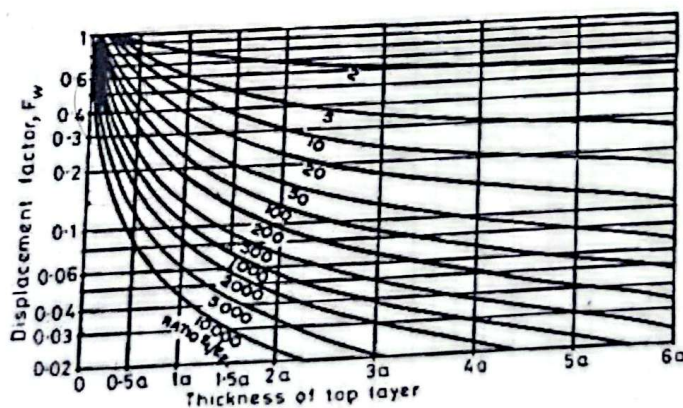
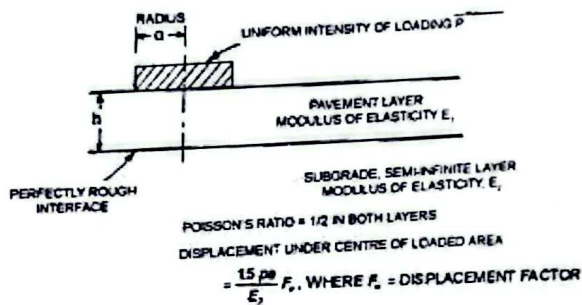


Two layer system

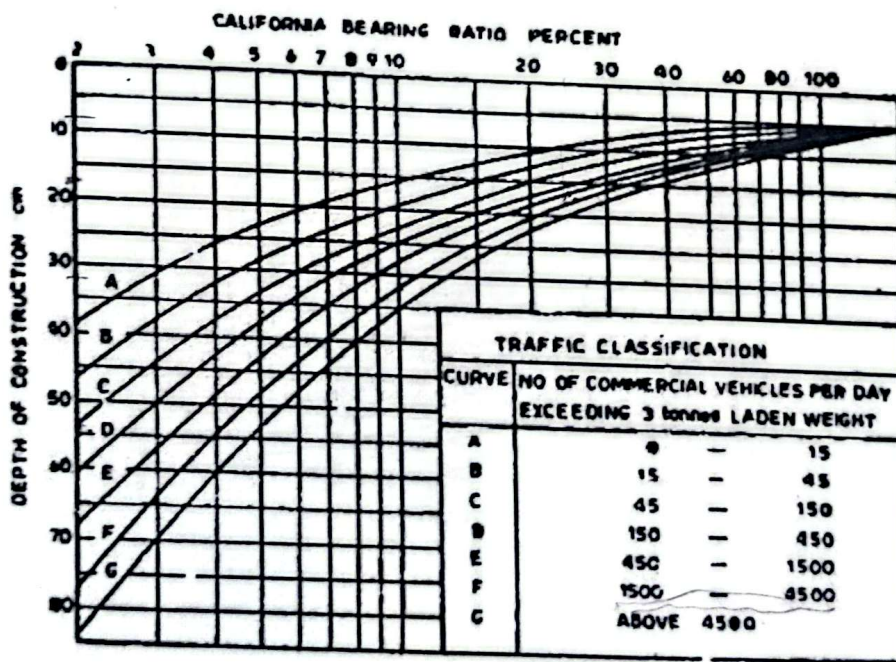
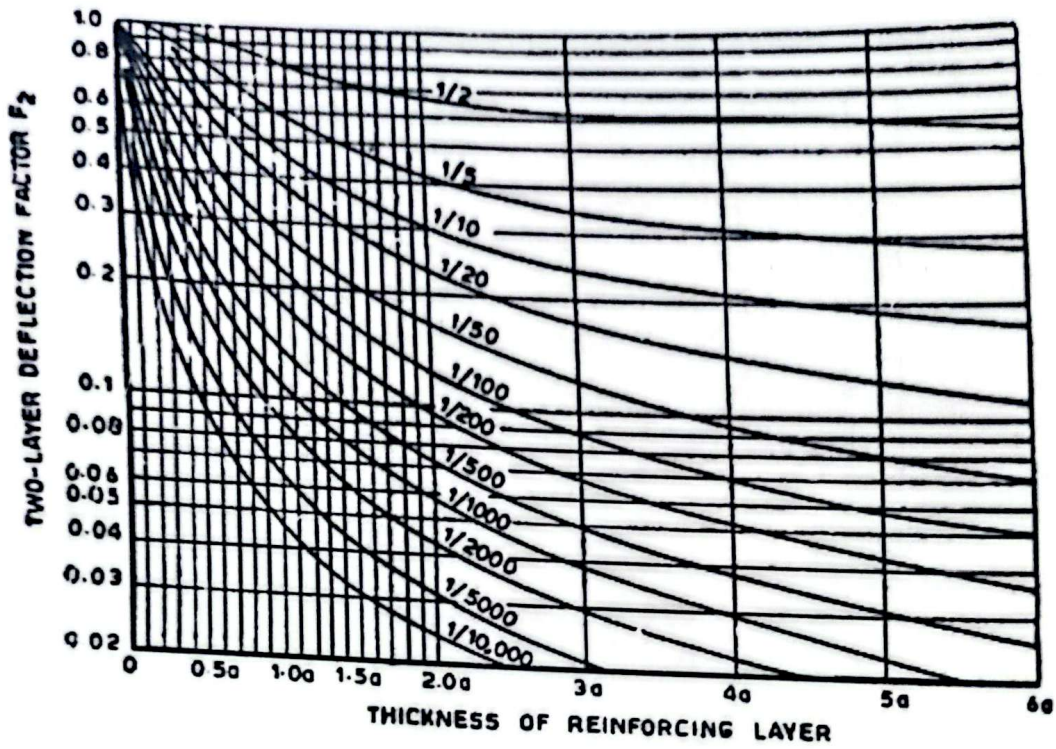
surface + base = 28 cm (---)
 * (Base only ⇒ subbase att's replace surf if a thickness of base diff's)
 Eq. thickness of 22 cm of subbase = 16 cm (---) base only
 15 cm (circled) 28 - 13 = 15 cm
 122 ⇒ 11 cm



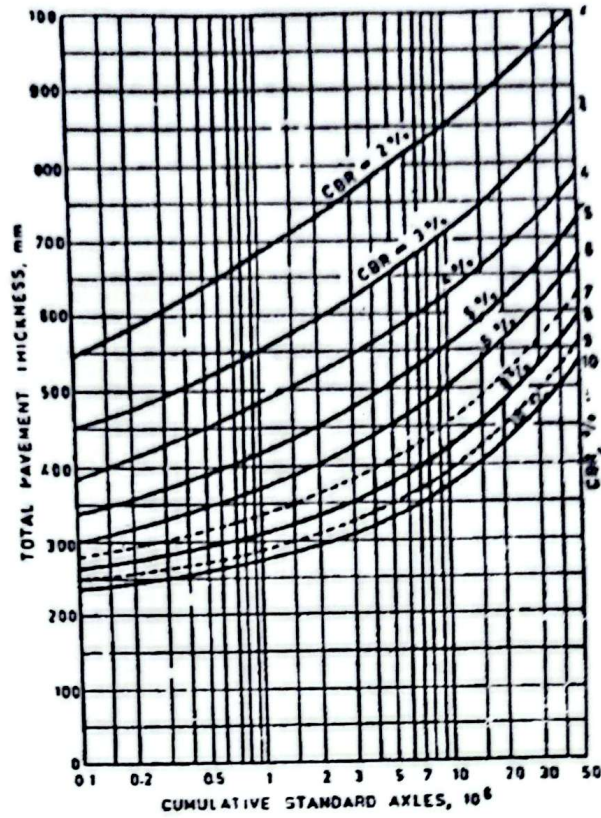
Boussinesq's theory pressure bulb shows, $\sigma_z \propto \frac{1}{z}$



Displacement factor (F_w): Boussinesq's theory.













IRC recommended CBR



Traffic classes	
Traffic classes	Range (10^6 esa)
T1	< 0.3
T2	0.3 - 0.7
T3	0.7 - 1.5
T4	1.5 - 3.0
T5	3.0 - 6.0
T6	6.0 - 10
T7	10 - 17
T8	17 - 30

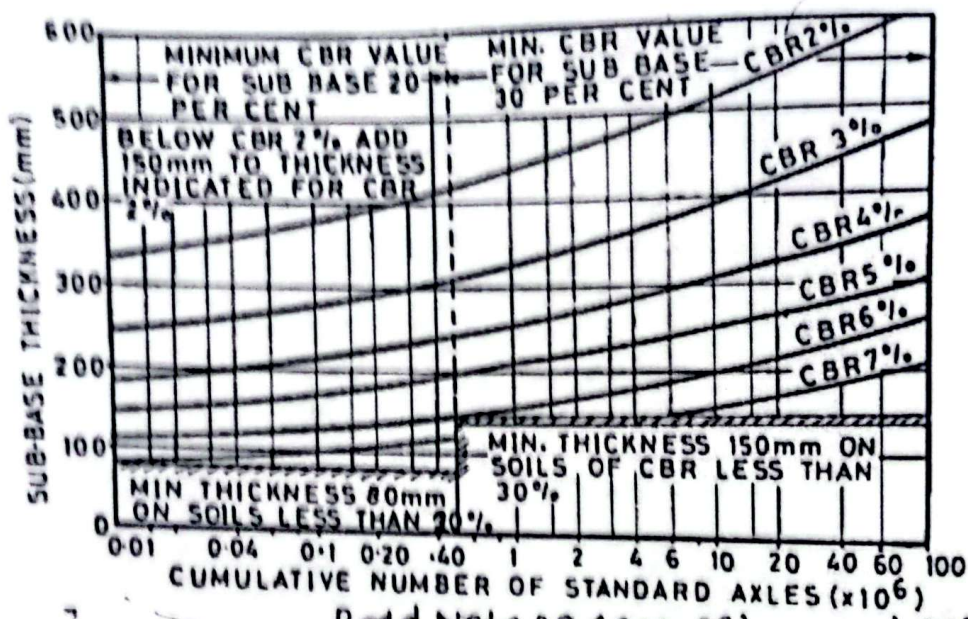
Subgrade strength classes	
Class	Range (CBR %)
S1	2
S2	3 - 4
S3	5 - 7
S4	8 - 14
S5	15 - 29
S6	30

Material Definitions

-  Double surface dressing
-  Flexible bituminous surface
-  Bituminous surface
(Usually a wearing course, WC, and a basecourse, BC)
-  Bituminous roadbase, RB
-  Granular roadbase, GB1 - GB3
-  Granular sub-base, GS
-  Granular capping layer or selected subgrade RL, GC
-  Cement or lime-stabilised roadbase 1, CB1
-  Cement or lime-stabilised roadbase 2, CB2
-  Cement or lime-stabilised sub-base, CS

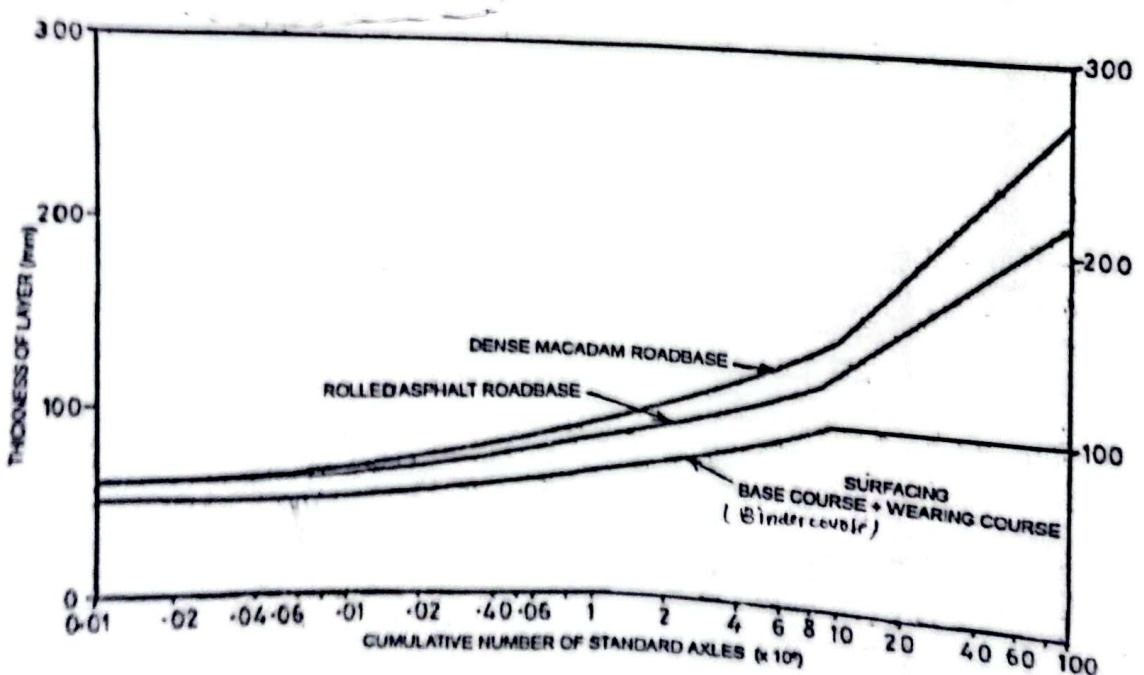
KEY TO STRUCTURAL CATALOGUE

Traffic classes (10^6 esa)	Subgrade strength classes (CBR%)
T1 = < 0.3	S1 = 2
T2 = 0.3 - 0.7	S2 = 3 - 4
T3 = 0.7 - 1.5	S3 = 5 - 7
T4 = 1.5 - 3.0	S4 = 8 - 14
T5 = 3.0 - 6.0	S5 = 15 - 29
T6 = 6.0 - 10	S6 = 30+
T7 = 10 - 17	
T8 = 17 - 30	

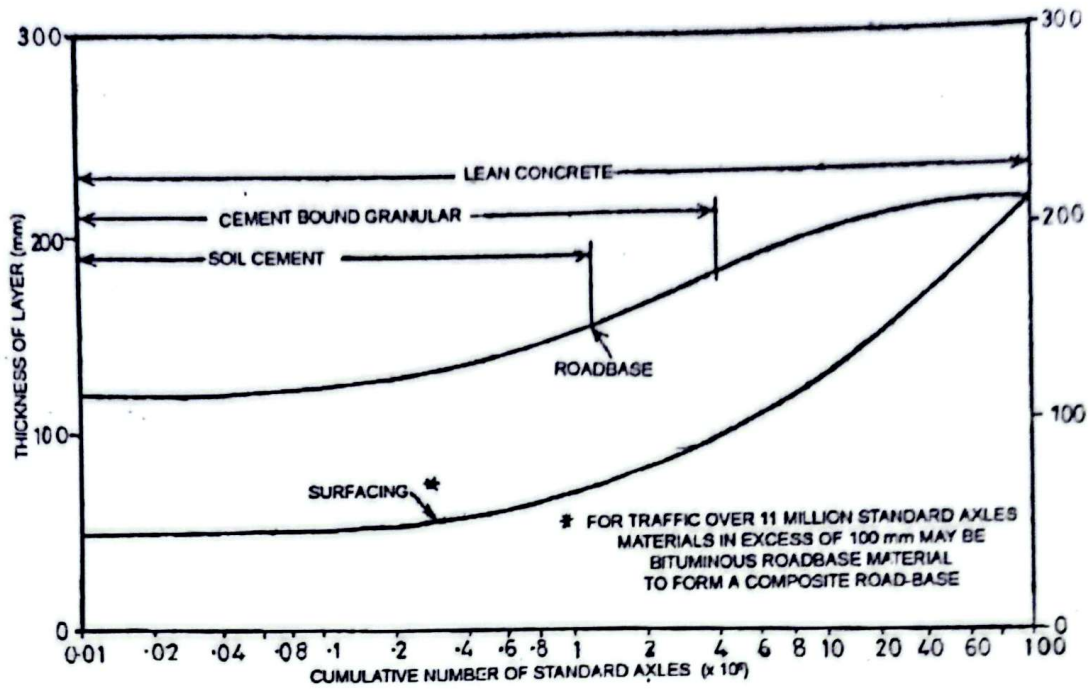


Road Note 29 (EN-29)

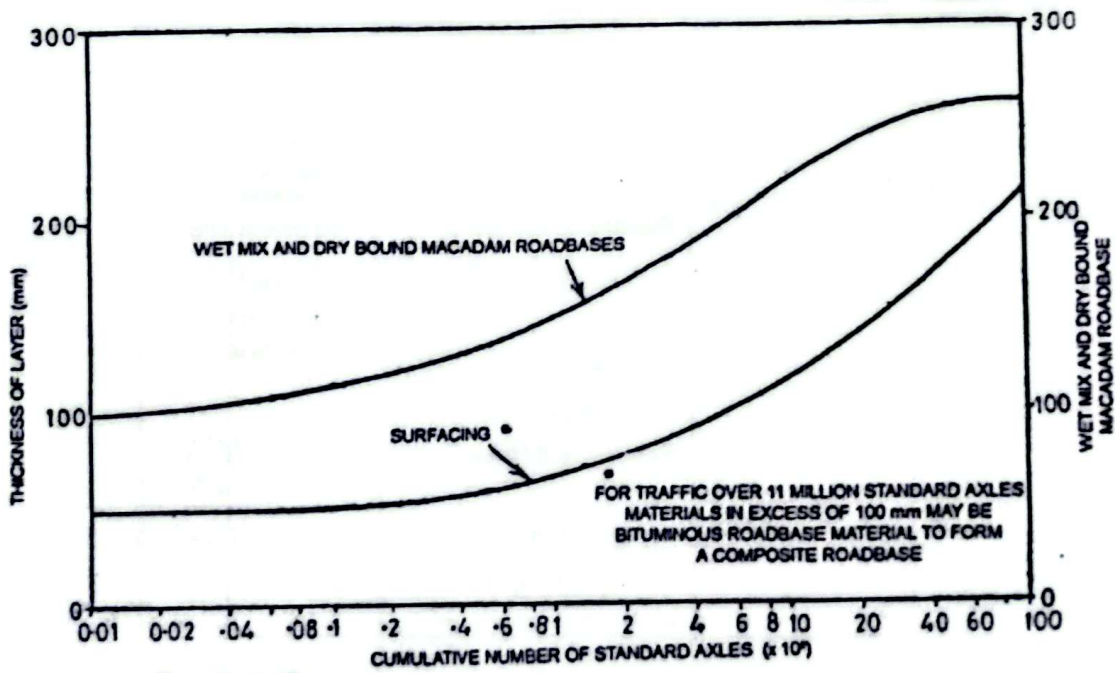
1 Million standard axles



• Rolled Asphalt base, dense Macadam base (chart 1)



lean concrete base, cement bound granular base,
soil cement base



Wet mixed and dry bound Macadam base.

- (2T) 3. Road construction Technology } Principles of Highway
- (STO7W) 4. Road Maintenance } Eng. L.P. Kadiyall,
- (1T) 5. Introduction to Bridge & Tunnel } Highway Engg. Khanna & Justo
- ↳ Transportation Engineering II - Vazirani
- 6. Some portion from Traffic Engineering
- (2N + 2T) ↳ Transport Planning & Traffic Engineering - Kadiyall, Khanna & Justo

- Transportation Engg. II Shrestha & Marasini
- Handouts

* Standard specification for Road & Bridge.

- Branch of engineering that deals with:
 - All activities for changing existing ground to the desired shape and slope
 - Providing all necessary facilities for traffic operation
 - Reconstruction/Maintenance of existing roads.

• Activities in road construction

1. Earthwork
2. Drainage
3. Pavement
4. Miscellaneous
 - Median
 - Road markings
 - Traffic sign
 - Footpath.
5. Slope stabilization

(1) Earthwork & site clearance

- site clearance
- Earthwork in filling for embankment
- ~~Exc~~ Excavation for cutting
- Excavation for borrow pit.
- Excavation for structure foundation

(2) Drainage works

- Minor bridges
- Culverts
- Causeways
- Side drains
- Catch drain

(3) Protection work

- site clearance
- River training works
- Gully control works
- Landline stabilization works
- Bridge protection works.

(4) Pavement works

- Sub-grade works
- Sub-base works
- Base works
- Surface works.

(5) Miscellaneous works

- Road ancillaries (Beautify road)
- Traffic sign/ signal/ marking etc.
- Bioengineering works.

Green roads → purely labor
↳ environmentally friendly and
↳ no use of equipments
↳ w/o disturbing environment.

3.2 Tools, Equipments & plants used in construction

(a). Tools

→ simple piece of equipment that we use to do a particular kind of work in construction, usually holding in hand.
→ Important for labor based construction.

- | | | |
|--------------------|----------------|-----------------|
| * Excavating tools | * Compaction | * Levelling |
| • Shovel | • Hammer | • Plumb bob |
| • Spade | • Rammer (एकल) | • Rope/staining |
| • Pick axe | | • Level pipe |
| • Crowbar | | • Spirit level |
| • Trowel | | • Trowel |
| • Hoe | | |
| • Chisel & hammer | | |

* Transport

- Wheel barrow
- Dokol Thunche
- Shovel
- Trowel

classmate
Date _____
Page _____

(b) Equipments

All appliances for the execution, completion, operation or maintenance of the road works but which will not become a permanent part.

→ Used for executing complex tasks in even the most unfavourable topography.
→ 15% to 40% of total project costs

- (1) - Earth moving (Excavating) equipment covers a broad range of machines that can excavate soil and rock.
- Earth movers help to speed not only earthwork but also
- ~~D~~DOZER (used for excavating at shallow depths.
- Scoopex (used to scrap surfaces. scrap old pavement during reconstruction)
↳ generally with blades & buckets
- Loader (for excavating as well as loading materials to other devices)
↳ with bucket that can be raised.
- Excavator (hoe is attached to boom
↳ for excavating trench, cleaning drains, etc.
↳ for excavating at different levels, below own level
- Backhoe (hoe at backward & loader at front operator)
- Dragline (used for excavation ⁱⁿ soft soil and sand at greater depth)

clams shell (excavation in underwater as it has clamp)
 (excavation at very different excavations)

dragging women
 ↑

(ii) Compacting equipments

- Refers to machinery used to compact soils, to increase the density of soil & reducing voids.

a. Smooth wheel roller

- used when the couching action (breaking down) action is required.

- roller with steel drum. Drum may be in one or two in number.

b. Sheep's foot roller

- used in compaction of cohesive soil i.e. clay & silt
 - steel drum with projection outward of diameter.

c. Pneumatic tyred roller

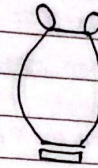
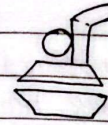
- work in kneading action (push and pull compaction)
 - May be 4 wheel - 3 wheel or 5 wheel - 4 wheel



d. Vibrating roller

- Steel drum with motor to generate vibration action which impare extra compaction/compression

e. Rammer



Monkey Jumper
 Used where heavy equipments cannot be used i.e. in side drains.

(iii) Levelling equipments

First levelling - Dozer

a. Grader

→ Precise levelling - Grader

→ has blades that can be tilted or adjusted at angles.

→ Used in forming camber, superelevation.

(iv) Lifting equipments → used when pre-cast elements have to be lifted.
 (e.g. huge pipes)

a. Crane

b. Hoist - to move people / material at different levels.

c. Forklift truck



(v) Paving equipment

(a) Bitumen spreader (distributor)

- spread bitumen at desired rate
- provided with bitumen storage tanks, nozzles & heating devices.
- to apply different coats i.e. prime coat, tack coat.
- rate of spreading of bitumen depends on size of nozzle's opening & speed.

(b) Aggregate spreader

- to spread aggregate at desired rate & thickness.
- rate of spreading depends on size of opening & speed of wheels.

(c) Bituminous paver

- to pave required thickness of bituminous concrete & bituminous mat.

(d) Cement concrete mixer

- only for small volume work.
- RMC for large volume work (Ready Mix concrete)

(e) Cement concrete paver

- to pave reqd thickness of cement concrete

(f) Concrete vibrator

- ↳ needle vibrator
- ↳ plate vibrator

(vi) Transport Equipment

(a) Haul truck

- for transport of hot mix asphalt

(b) Tipper

- bucket can be hydraulically lifted up & down

(c) Dump truck

- high capacity large volume.
- used in quarry site

(d) Trailer

- Power driven unit is coupled with non-power driven unit to transport equipment.

(e) Mini dumper

- to transport small volume of work in site

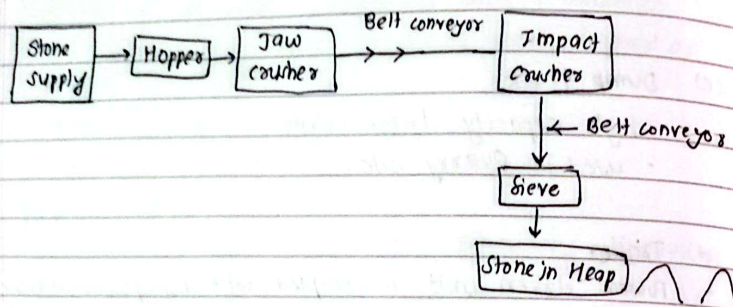
(f) Concrete transport truck

(RMC को जाती)

(c) Plants

- are fixed in site: unmovable
- combination of different equipments performing different action & fixed in a space.
- for complex, voluminous production work.

i. Stone crusher



ii. Asphalt Mixing Plant

iii. Cement concrete Mixing Plant

3 Preparation of Road Bed

- All operation before the pavement would be laid:

This includes:

(i) Site clearance

- clearing bushes and shrubs at least covering toe width
- Removal of existing trees, stumps and roots along the alignment
- Removal of existing structures along the alignment
- a minimum of 1 to 3m from the top of the cut or toe of the fill.

ii) Earthworks in Excavation (Cut)

- cutting and removing the earth, rock from its original position, transporting & dumping
- Required when the natural ground is higher than the designed level.
- Also construction of side drain require excavation

• Design:

- Depth
- stability of foundation
- stability of slope
- Requirement of side drains.

- (iii) Earth work in embankment (Fill)
- The filling of earth/soil to achieve the desired formation level
 - Required when the natural ground is below the formation level, high water table & prevent capillary rise

Design elements:

- Height of fill
- Fill material ($PI > 45$)
(swelling index 50%)
- Settlement of embankment
- Stability of foundation
- Stability of slopes

☞ → site clearance → materials dumped along alignment →

If $MC < OMC$ add moisture

If $MC > OMC$,
 → add petrol & burn
 → leave in situ it will dry up

(st. $MC \approx OMC$)

Spreading ← Compaction

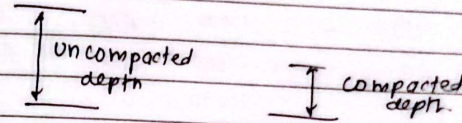
(One layer compacted thickness not more than 15cm)

For embankment depth	Compacted density
< 3m	15 kN/m ³
> 3m	17 kN/m ³

Mass-Haul Density Diagram

- ↳ Diagrammatic representation of earthwork volume involved in road construction along a linear profile.
- ↳ Horizontal stationing is plotted along the X-axis
- ↳ Net cut values are plotted above the X-axis (positive Y-value) & net fill values are plotted below X-axis (-ve Y-value)

Steps: (i) compute the net earthwork value for each station, applying the appropriate shrink factor.



Shrinkage:

- ↳ volume of the compacted embankment is less than the borrow area volume, called shrinkage
- ↳ Shrinkage factor depends on soil type & vary between 10-20%.

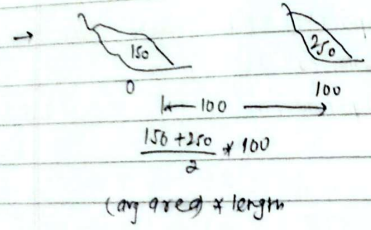
Swell:

- ↳ Excavated soil/rock occupy a larger volume, called Swell.
- ↳ Swell may vary from 20-40%.

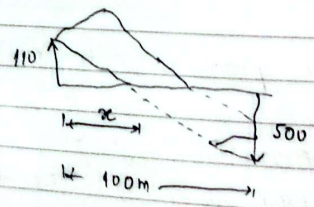
- (ii) Net cuts have a positive value, net fill have a negative value.
- (iii) The value at the first station (origin) = 0
- (iv) Plot the value of each succeeding station, which equals the cumulative value to the point.

Plot the mass haul diagram for the earthwork quantities contained in table.

Station	Area		Volume		Cumulative Earthwork
	cut	Fill	cut	Fill	
0	150	-	0	0	0
100	250	-	20000	0	20000
200	110	-	18000	0	38000
300	-	500	2750	-12500	28250
400	-	170	0	-33500	-5250
500	-	350	0	-26000	-31250
600	480	-	12000	-8750	-28000
700	20	-	25000	0	-3000
800	220	-	12000	0	9000
900	10	-	11500	0	20500

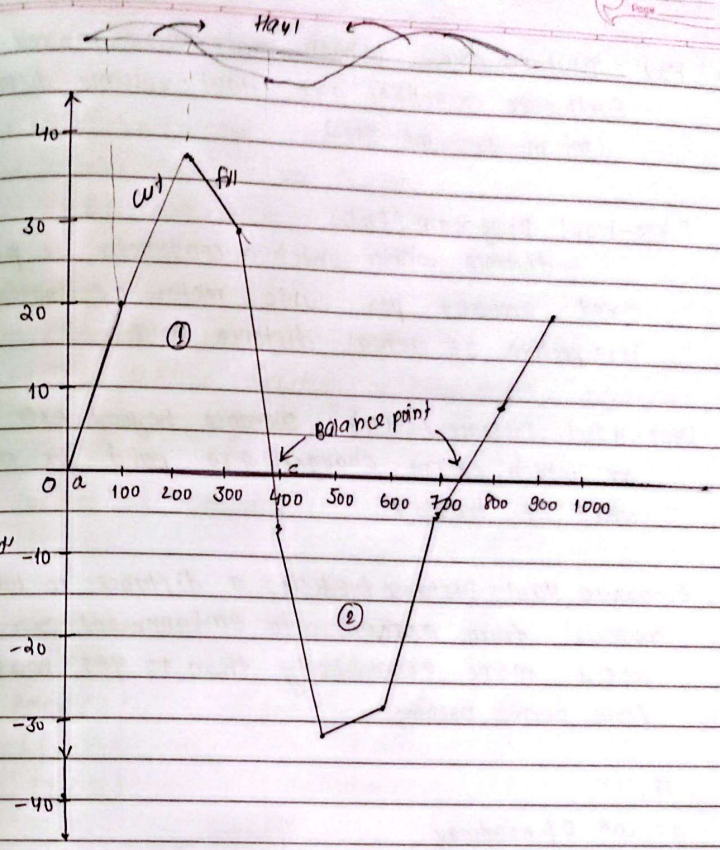


→ 300 → cut & fill के बीच का क्षेत्र
at some pt. it will be zero
इसका क्षेत्र? ⇒ interpolation.



say (assume) → distance zero क्षेत्र
say, $x = 50m$. (अनुसार ground condition)
but, not give exact value!

(slide mass)



① convex
② concave
at → zero balance line

• Haul: Distance over which material is moved.
 Earthwork quantities are Haul · volume · distance
 ($m^3 \cdot m$ or $m^3 \cdot \text{Sta.}$)

• Free-Haul Diagram (FHD)
 A distance within which a contractor is paid a fixed amount per cubic meter of material irrespective of actual distance price.

• Over-Haul Distance (OHD): Distance beyond free-haul for which extra charges are paid for each unit of haulage.

• Economic Haul Distance (EHD): a distance to which material from excavation to embankment can be moved more economically than to get material from borrow opening.

If,

a = cost of roadway excavation per m^3

b = cost of overhaul & tipping per m^3/m

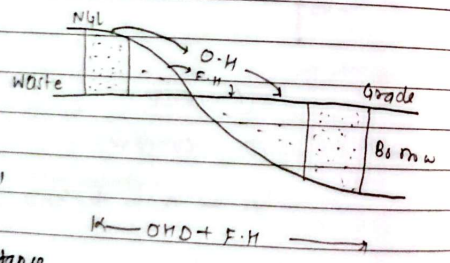
c = cost of borrow material per m^3

L = economic overhaul distance in m

Cost of overhaul = cost of borrow

$$a + bL = a + c$$

$$\Rightarrow L = \frac{c}{b}$$



3.4 construction of low cost roads

- Low construction cost & maintenance cost
- Suitable for low vol. traffic.
- WBC earthen road.

Earthen roads:

- cheapest road
- It utilize existing or immediately adjacent materials along an alignment.

section of Materials:

	Bare course	Wearing course
clay (%)	< 5	10-12
silt (%)	9-32	5-15
sand (%)	60-80	65-80
LL (%)	< 35%	< 35%
PL (%)	< 6%	4 to 10%

□ 3.4.3] Water Bound Macadam Roads

- pioneered by Scottish Engineer John Loudon Macadam around 1820
- Made of crushed gravel, hard stones, etc.
- The broken stones are mechanically interlocked by rolling
- The voids filled with ascending & binding material with the assistance of water.

• Selection of materials:

- Angular and cubical shape, nominal size Grading 1 (63mm), Grading 2 (53mm), LA value upto 40% (base) & 45% (subbase), ATV upto 30% (base) & 40% (subbase) and combined flakiness & elongation index less than max 35%.

- screening materials (Grading 1 - 13.2 mm, & Grading 2 - 11.2 mm) of LL < 20%, PL < 9%.

- Filler (Binding) materials fine graded material, Plasticity Index less than 6%.

• Equipments:

Water tankers, dump truck, grader, compaction equipment.

• Construction process:

- Material with 20% extra broken stones are stocked along the road.
- Preparation of subgrade to required grade & camber
- Provision of lateral confinement:

- spreading of CA
- Dry rolling - roller 8 to 10 tonnes (compacted thickness 5-7 cm) three wheeled power rollers or tandem or vibratory rollers
- Dry screening is applied gradually over the surface to fill the voids
- The surface is sprinkled with water and wet rolling to fill about 50% of total voids.
- Application of binding material at a uniform and slow rate of two and more thin layers.
- opening of traffic after few days of construction.

Quality Control:

- Material specification
- LAA, PI, Flokin and Elongation Index
- 90-10% of OMC.
- Dry density = 95% of MDD, 95% for subbase and shoulder.
- Plasticity Index 6 for base course and 5 to 10 for surface course.

3.4.4 Soil Stabilization

↳ process of improving the strength of the soil by proportioning and/or mixing with other material & compaction.

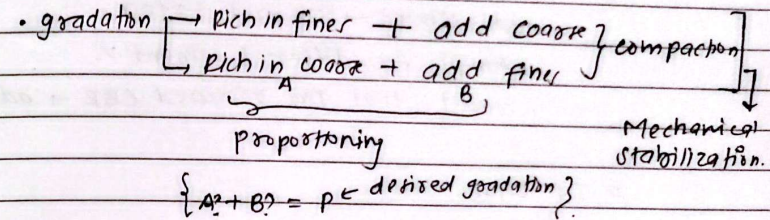
Advantages

- Increase bearing capacity of soil
- Increase shear strength of soil
- Avoid changes in soil characteristics due to changes in moisture content
- Prevent cracks in soil.

→ Good drainage, less frost susceptibility.

Basic principle in soil stabilization

- Evaluating the properties of soil
 - gradation, soil type (Clay, sand), PI
- Deciding the effective and economical method of soil stabilization.



• gradation + cement → when soil has ^{sufficient} granular materials (but PI & plasticity property is weak)

• gradation + Lime → when soil has sufficient clay. (PI of clay ↓ + stabilization)

sand (cohesionless) → Bitumen.

c) Designing mixes

[Mix % of soil add what?]

(i) Proportioning Method

Proportion of A & B to find required gradation.

(ii) Mixing

@ If cement.

↳ decide from compressive strength

Req^d value 17.5 kg/cm² → light traffic
35 kg/cm² → heavy traffic

How?

5cm ϕ & 10cm height cylinder

+ compaction

+ curing (7 days)

(trial cement %) \rightarrow \uparrow σ_{CBR} with st. org.
Compressive strength
& not

⑤ CBR Test

add cement \rightarrow compact \rightarrow test.

• sample for different cement %.

• cement % that give required CBR \rightarrow adopt.

If Lime

① PI value

② Lime fixation limit

③ CBR.

+ curing + 14 day.

① PI value \rightarrow % lime that gives PI value within upper limit.

② (Lime add, PL \uparrow upto a limit then PL \downarrow in further \uparrow in lime, at that point which is called fixation limit and lime at that level taken as % lime).

% lime that doesn't increase PL value (plastic limit)

③ % lime that gives required CBR

If Bitumen

(used in sandy (cohesionless soil))

- CBR.

(iv) \rightarrow Compacting the stabilized soil adequate

Surface Dressing (Surface Treatment)

→ The application of bituminous emulsion over the prepared road base followed immediately by covering with single sized stone aggregate chippings that are lightly rolled.

(first lay bitumen followed by aggregate)
eg. Surface Dressing

- ↳ single bituminous surface treatment (SBST)
- ↳ Double bituminous surface treatment (DBST)

• Equipment

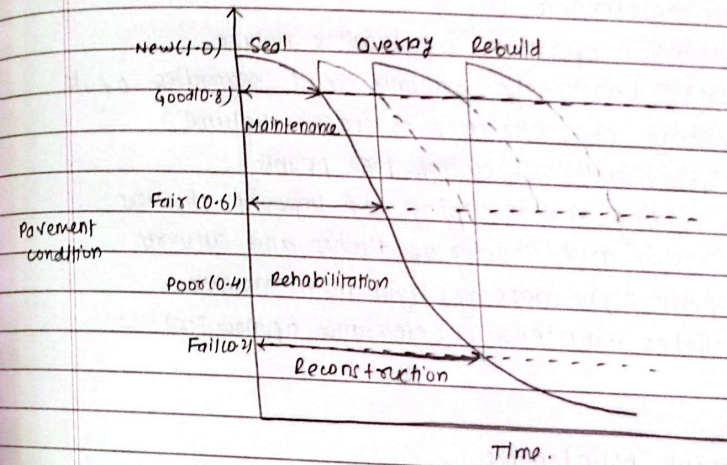
• Construction Procedure (SBST)

→ surface cleaning by sweeping with mechanical brooms

Ch 4 Highway Maintenance, Repairs and Rehabilitation

- Highway maintenance is preserving and keeping the serviceable conditions of highway as normal as possible and as best as practicable.
- eg. sealing of cracks, filling pot holes, etc.
- Highway Rehabilitation is improving the structural strength of pavement.
- eg. Overlay of greater thickness, replacement of surfacing, etc.

* Concept of Pavement maintenance



* Classification of Maintenance activities

- ↳ Road maintenance
- ↳ Roadside maintenance.

• Road Maintenance

- All maintenance works on the road way
- Maintenance of all structures within road way (eg. side ditches, culverts, causeways, bridges, etc.)

- Types:

- Routine Maintenance
- Recurrent Maintenance
- Periodic Maintenance
- Emergency Maintenance

- Routine maintenance

- ↳ Maintenance operations of localized nature
- ↳ Require continually on any road regardless of its engineering characteristics or traffic volume.
 - Grass and bush cutting, tree pruning
 - Grading and reshaping of unpaved shoulders.
 - Clearing and cleaning of ditches and culverts
 - Road sign, marking, light maintenance, etc.
 - Winter maintenance (clearance of snow, ice)

- Recurrent Maintenance

- ↳ Maintenance operation of localized nature carried out at more or less regular interval of six months to two years with a frequency that depends on the traffic volume.
- ↳ to be done by using minor equipment
 - Sealing cracks
 - Local surface treatment
 - Repair of depressions, holes and surface hole patching, etc.

- Periodic Maintenance

- Maintenance operations of large extent required only at intervals of several years
- Frequency and type depend on original surfacing, traffic, rainfall and climatic conditions
 - Resealing (surface treatment, slurry seal, thin overlay)
 - Re-gravelling of unpaved road
 - Restoration of road marking, drainage items, etc.

- Emergency Maintenance

- ↳ Urgent emergency maintenance works needed for reopening of road after slides, road wash out, etc.
- ↳ Removal of debris or any other obstacles.
- ↳ Reinstatement of the pavement structures and drainage after rainy season.
- ↳ Strengthening/reconstruction of pavement.
- ↳ Protect road against fall of rock, flooding, etc.

- Road side maintenance
 - concerns all maintenance works on structures and surface above and below the road having direct active and/or passive influence on the road.

- E.g. culverts protection works, retaining walls, cut slopes, fill slopes, unstable natural slopes, river protection works and vegetation structures.

Inspection, prioritization and planning of maintenance operations

- Type and extent of maintenance depends on.
 - Serviceability standard
 - Maintenance fund available
 - Priorities for the maintenance operation.

* Inspection and Assessment of maintenance need.

- Find out road inventory (soil type, terrain, climate, etc.)
- Nature and volume of traffic.
- Identify defects likely to be hazardous or cause serious inconvenience to users of the highway.
- Identify defects requiring urgent attention.
- Priorities are determined through regular inspection of each road usually the six months.

* Prioritization of maintenance operations

- Urgent repairs (eg. removal of debris)
- Routine drainage work (Ditch cleaning, cleaning of culvert bridges, filling scour areas, etc.)
- Routine pavement work (grading of unpaved road, patching, sealing of paved roads)
- Shoulder maintenance, grass cutting, cleaning and repairing road furniture.
- Periodic work like grading, re-graveling of unpaved road, surface dressing, etc.
- Overlay and reconstructions.

* Planning of Maintenance operations

- Minimum acceptable service standard
- Field survey for finding maintenance requirement.
- Factors influencing maintenance need such as sub grade, drainage, traffic, environment.
- Estimate extent of pavement deterioration.
- Development of alternatives of maintenance.
- Check availability of funds, materials, manpower and equipment
- Maintenance costs.

Type of Road Failure and its cause

1. Failures in flexible pavements
2. " " rigid "

1. Failure in flexible pavements

• Flexible pavement failure

- ↳ Excessive deformation/settlements of any layers
- ↳ Excessive undulation or waves and corrugation.
- ↳ Lateral shoving of the pavement near the edge along the wheel path

(i) Failure of sub grade

Causes

- Inadequate stability or strength
- Excessive stress application.

(ii) Failure of sub-base or Base

Causes

- Inadequate stability or strengths
- Loss of binding action
- Loss of base course materials
- Inadequate wearing course
- Use of inferior materials
- Lack of lateral confinement for the granular base course.

(iii) Failure of wearing course

• Causes:-

- Improper mix design
- Inadequate quality control during construction
- Volatilization and oxidation of bitumen.

* Typical Flexible pavement failures

(a) Alligator (map) cracking:

- Due to fatigue, localized weakness in base course would also cause such cracking.
- Because a structural failure is taking place, the only possible solution is a full-depth patch.

(b) Rutting:

- Channelized depressions along the wheel-path
- Due to consolidation, lateral movement of any pavement layers.
- Insufficient pavement thickness and compaction.

(c) Longitudinal cracking

- Parallel to pavement centerline
- Due to frost action, differential volume change, and/or poor joint construction.
- Crack $< \frac{1}{2}$ inch can be sealed
- Severe cracks - ~~to~~ remove the cracked pavement layer and replace it with an overlay.

(d) Reflection cracking

- Observed in a flexible pavement over a rigid pavement
- occur directly over the underlying rigid pavement joint or over cracks in rigid pavement
- crack sealing for cracks less than 1/2 inch, and removal of the cracked pavement layer followed by an overlay for severe one.

(e) Pot holes

- small, bowl-shaped depressions in the pavement surface that penetrate up to the base course.
- Due to moisture infiltration and usually the end result of untreated alligator cracking.
- Full depth - replacement patch.

(f) Ripples (corrugations) and wave (shoving):

- Rippler or an abrupt wave across the pavement surface.
- usually occur at points where traffic starts and stops
- caused by excess asphalt; too much fine aggregate; rounded aggregate; too soft an asphalt; or a weak granular base.
- small - distortion - patching, For large - overlay.

(g) Slippage cracking

- slipping occurs when the surface is not bound with the underlying layer or low strength surface mix.
- slowly, it forms pot holes
- Fix: Removal and replacement of affected area.

(h) Shear failure

- Excessive loads that cause a shear failure in the subgrade, base course, or the surface.
- characterized by upheaval of pavement followed with depressions
- Fix: Removal & replacement of affected area.

(i) Raveling

- The separation of aggregate particles in a pavement
- usually, the fine aggregate wears away first. Soon larger and larger particles are broken free.
- Due to loss of bond between aggregate and bitumen.
- Fix: small raveling - patching, for large raveled area a thin hot-mix overlay.

(j) Frost Heaving

- localized heaving up of portion of pavement due to action of frost.
- small distortion - patching for large - overlay.

(k) Polished aggregate

- Areas of pavement where there are no rough or angular aggregate particles, loss of skid resistance
- Due to abrasion of soft aggregates
- Fix:- abrasion free overlay.

2. Failure in Rigid Pavements

- Formation of cracks is the main cause of failure.
- They fail mainly due to two factors:

• Deficiency of pavement material:

- Soft aggregate
- Poor workmanship in joints
- Poor joint filler and sealant material
- Poor surface finish
- Improper and insufficient curing.

• Structural inadequacy of pavement:

- Inadequate pavement thickness
- Inadequate sub grade supports and poor sub grade soil
- In correct spacing of joints

* Typical Rigid Pavement Failures:

(i) Scaling of cement concrete:

- The deterioration of the upper concrete slab surface
- Deficiency in mix or presence of chemical impurities
- Excessive vibration makes mortar on top of the layer which get abraded exposing aggregate
- Repairs with bituminous patch or cement mortar

(ii) Shrinkage crack

- Hairline cracks formed during concrete setting and curing that are not located at joints.
- Due to poor reinforcement, improper curing technique, high early strength.
- For moderate, cracks are sealed; for severe slab replacement

(iii) Spalling of joints

- Loose debris on the pavement, roughness, generally an indicator of advanced joint/crack deterioration.
- Excessive stresses at the joint/crack, low quality concrete
- Disintegration of the PCC from freeze-thaw.
- Repairs: Partial or full depth patch.

(iv) Warping crack

- For improper design of joints, irregular cracks are developed at joints due to excessive warping stresses
- Hinge joints are provided with adequate reinforcement

(v) Corner crack

- A crack that intersects the PCC slab joints near the corner
- Severe corner stresses caused by load repetitions combined with a loss of support, poor load transfer across the joints, curling stresses and warping stresses
- Repair: Full depth patch

(vi) Mud pumping

- Movement of material underneath the slab or ejection of material from underneath the slab
- Due to repeated occurrence, slab loses subgrade support
- Water accumulation due to a high water table, poor drainage, and cracks or poor joint seals that allow water to infiltrate
- Full depth patch to remove any deteriorated slab area & stabilize subgrade

(vii) Pop-out

- Small pieces of pavement broken loose from the surface
- Causes: Use of non-durable aggregates, Improper curing, Internal pressure

(viii) Blow out

- A localized upward slab movement and shattering at a joint or crack
- The result of insufficient room for slab expansion during hot weather
- Full depth patch

(ix) Polished aggregates

- Surface mortar and texturing worn away to expose coarse aggregate resulting skidding surface
- Due to abrasion of soft aggregates
- Fix: abrasion free overlay

Types and methods of pavement repair

1. Maintenance of Earthen/Gravel Roads
2. " " WBM "
3. " " Bituminous "
4. " " Cement concrete "

1. Maintenance of Earthen/Gravel Roads

• Common problems

- Formation of dust
- Formation of longitudinal/cross ruts along the surface.

• Maintenance

- Maintained by sprinkling water, treatment with calcium chloride, applying oiled earth to prevent dust
- Periodic maintenance by spreading moist soil (gravel) along rut and reshaping of the camber or suitable stabilizing treatment is provided on surface.

2. Maintenance of WBM roads

• Problems

- Dust formed in dry weather, mud in rain
- Pot holes and ruts.

• Repairs

- Dust is reduced by sprinkling dust palliatives, moist soil or bitumen spreading.
- Spreading of a thin layer of moist soil binder on the surface periodically to prevent aggregate disintegration.
- Pot holes and ruts are remedied by patch repair.
- Cut defective area in a rectangular shape up to defective depth.
- Coarse aggregate of same size as old is filled up and compacted up to 1cm.
- Wet soil binder is applied on the surface of the patched area and surface rammed again.
- Resurfacing after its useful life.

3. Maintenance of Bituminous surfacer

• Repair works mainly consists of:

- Patching

- Surface treatments

- Repair of depression and settlement of pavement and shoulder.

- Repairs of pavement edge and shoulder distress

- Resurfacing

* Patch Repair

• Patching

- Potholes or other defects in the road surface shall be cut to rectangular shape.
- Excavate the area until sound materials encountered.
- Clean area by removing dust and loose materials.
- Apply prime tack coat at side and bottom of area.
- Premix material is placed in layers of 6cm quarterly.
- Compaction is carried out.
- Patch repair should be slightly higher than old pavement.

* Surface treatment

• Surface treatment

- Bleeding

↳ corrected by application of blotting materials such as chips (10mm), sand, etc. and rolling.

- Cracks

↳ Bituminous surface treatment renewal coat.

↳ More than one layer of surface treatment may be necessary if surface is severely damaged.

- Skidding surface

↳ skidding occurs as a result of polishing of aggregate by wheel

↳ Bituminous surface treatment renewal coat

- Sweeping the surface area clean by broom
Mechanical broom sweepers

- Mark out the area to be repaired in box shape
- For small area of the cracks, compacted with vibrating plate. And, for large area use hand roller compactor.

* Resurfacing

- If pavement surface is totally worn out and develops poor riding surface, additional surface course is provided on the existing surface.
- If thickness is inadequate, overlay of adequate thickness should be designed and constructed.

* Rut, corrugation and wave repair

- Necessary to correct the defect such as excessive moisture, poor compaction, etc. in any pavement layers.
- If instability due to excessive moisture, suitable sub surface drainage is necessary.
- If failure is due to improper compaction, it needs complete reconstruction

→ Marking out the area to be repaired

→ Clean area to be repaired by using mechanical broom or hand broom

→ Spray tack coat (0.5 to 1.4 m²) and spread aggregate 19mm.

→ Compaction using tammer or vibrating plate compactor

- Apply binder over the surface.
- Distribution of aggregate 1mm scattered by shovel from the truck or trailer.
- Compaction using rammer or vibrating plate compactor.

4. Maintenance of cement concrete roads:

- Little maintenance is necessary
- Mainly maintenance of cracks and joints.
- Maintenance of cracks:
 - Non-structural cracks:
 - hair cracks, shrinkage cracks, warping cracks
 - Structural cracks:
 - mostly appearance on the edge and corner regions due to load and warping stresses.

* Maintenance of non-structural cracks:

- Hairline cracks are harmless. However, if wider, it allows infiltration of water.
- They should be seal off to prevent entering the water
- The cracks are thoroughly cleaned using a sharp tool; stiff brush and air compressor.
- kerosene oil is applied for better bond.
- The cracks are filled with bituminous seal.
- Sealer is placed 3 mm above the level and layer of sand is spread over it for protection.

* Maintenance of structural cracks

- Need immediate attention
- Cause of failure are investigated and remedial measures are taken.
- For localized failure which may be due to settlement, re-casting of slab is done.
- General structural cracks, provide a flexible or rigid overlay
- Reconstruction of new flexible or rigid pavement if pavement is badly damaged.

• Joint Maintenance

- opened up joints are cleaned with brush or air compressor
- Refill the suitable sealer before start of the rain.
- Replacing the filler and sealer materials.

• Maintenance of Mud pumping

- Provide effective sub-surface drainage
- localized failure, patching of portion of slab (either asphalt or concrete)
- Mud jacketing & uplift of slab
 - ↳ Drill number of holes about 5cm dia and about 1 to 3m apart.
 - ↳ Grouting of 1:3 cem. sand mix, (cement:oil), or bitumen under pressure
 - ↳ slabs are raised upto desired ht. by pressure.

□ Evaluation of Pavement Distress and Pavement Condition:

- Assess the existing conditions and find out pavement service condition so that the maintenance and strengthening works can be planned on time.
- It covers a thorough study of various factors such as:
 - > Subgrade support
 - > Pavement composition and its thickness
 - > Present traffic loading
 - > Environmental conditions

- The method of pavement evaluation:

- Structural evaluation of pavements
- Evaluation of pavement surface condition (Functional Evaluation)

* Structural Evaluation of Pavement

- structural condition is concerned with the structural capacity of the pavement i.e. whether the pavement is structurally capable for design traffic, and climatic condition.
- Structural capacity measured by deflection, stresses, strain at critical points in pavement layers under the application of load. Also layer thickness, and material properties are also studied.
- Benkelman beam is commonly used, where deflection of pavement under standard load of 8.2 tons is used to find pavement overlay thickness.

* Evaluation of pavement surface

- Concerned with the ride quality or surface texture of a highway section.
- Pavement may be evaluated by the traveling, rutting, patches, cracks and surface roughness.
- Evaluated by Present Serviceability rating, surface distress index (SDI), and International roughness index (IRI), skid resistance, etc.

Strengthening of existing pavements

- After maintenance, pavement should have adequate stability to withstand the design traffic under prevailing climate and sub-grade conditions.
- If the pavement have to support increased wheel loads and more load repetitions, strengthen of the existing pavement is required.
- Strengthening required additional thickness of pavement, which is called overlay

* Overlay

- One or more layers of bituminous or cement concrete construction on an existing pavement.
- The overlay generally includes a levelling course to correct surface irregularity of the old pavement, followed by an overlay of uniform thickness.
- The type of material for overlay design depend on factors such as:
 - Importance of the road
 - Design traffic
 - Thickness, and condition of existing pavements
 - Construction convenience
 - Economical

• Types of overlay

S.No.	Existing Pavement	Overlay
1	Flexible	Flexible
2	Flexible	Rigid
3	Rigid	Flexible
4	Rigid	Rigid

- 1.
- CBR value of subgrade soil is determined
 - Total design thickness of the flexible pavement for the design traffic volume is determined.
 - The existing thickness of pavement is found from test pits
 - Total overlay thickness

$$h_o = h_d - h_e$$

where,

h_o = overlay thickness required, cm

h_d = total recent design thickness, cm

h_e = thickness of existing pavement, cm

4.

- Total overlay thickness

$$h_o = (h_d^a - x h_e^b)^n$$

where,

h_o = overlay thr. reqd, cm

h_d = total recent design thr, cm.

h_e = thr. of existing thickness, cm

values of a, b, x and n depend on pavement and the method of overlay construction.

Agency	Existing Pavement condition	X
Coops of Engineers and PCA	(i) Good condition	1.00
	(ii) Initial cracking	0.75
	(iii) Badly cracked	0.35

Agency	Construction period	a	b	n
Coops of Engineers	(i) Poured directly on old pavement	1.40	1.40	1/1.4
	(ii) Levelling course	2.20	2.0	1/3
PCA	(i) as (i) above	1.87	2.0	1/2
	(ii) as (ii) above	2.20	2.0	1/2

- 3.
- wheel load distributed over large area
 - Wearing stresses reduced.
 - Total overlay thickness given by

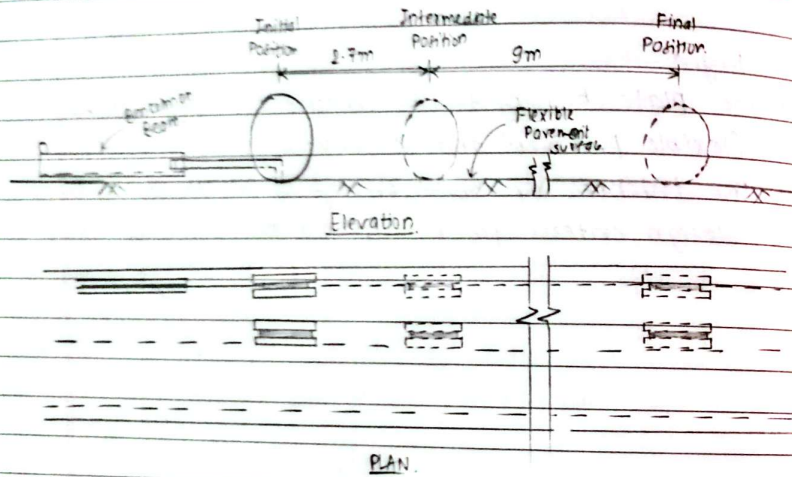
$$h_o = 2.5(F h_d - h_e)$$

F → factor which depends upon modulus of ~~etc~~ existing pavement

2. Rigid

- The plate bearing test is conducted on the existing flexible pavement and K value is obtained.
- The thickness of rigid overlay is calculated by using design criteria for rigid pavements

- # Deflection approach of overlay Design
- The structural strength of pavement is assessed by measuring surface deflections under a standard axle load (8.2 ton)
 - Larger pavement deflections imply weaker pavement and subgrade
 - The overlay must be thick enough to reduce the deflection to a tolerable amount
 - Rebound deflections are measured with the help of a Benkelman Beam.



* Loading and other standards

→ Axle load of 8170 kg

* No. of Deflection Measurement

→ At least 10 deflection measurements are made each section per lane subject to a minimum of 20 measurements per km.

→ If the highest or the lowest deflection values for the section differ from the mean by more than one-third

of the mean, then extra deflection measurement should be made of 25m on either side of point where high or low values are observed.

* Loading and other standards

→ Axle load of 8170 kg / load of 4085 kg on dual wheels

→ Tyre pressure, $p = 5.6 \text{ kg/cm}^2$

→ Standard pavement temperature = 35°C

→ Highest subgrade moisture content soon after monsoon.

→ Variation of individual values, not more than one third of mean value.

* Other Data measured

→ Measurement of pavement temperature (at one hour intervals)

→ Measurement of field moisture content of subgrade soil.

→ Typical subgrade soil samples for lab. Tests (soil classification)

→ Annual rain-fall.

→ Traffic data, growth rate, axle load data, VDF values.

* Analysis of Data

→ If $(D_i - D_f)$ is less than 0.025 mm (2.5 div),

$$D = 0.02 (D_0 - D_f), \text{ where } D \text{ in divisions } [1 \text{ div} = 0.01 \text{ mm}]$$

→ If $(D_i - D_f)$ is more than 0.025 mm (2.5 div),

$$D = [0.02 (D_0 - D_f) + 0.0582 (D_i - D_f)]$$

where D in divisions [1 div = 0.01 mm]

$$D = 0. [2 (D_0 - D_f) + 2 \times 2.91 (D_i - D_f)], \text{ where } D \text{ in mm.}$$

• Mean deflection, $\bar{D} = \frac{\sum D}{n}$

• Standard Deviation, $\sigma = \sqrt{\frac{\sum (D - \bar{D})^2}{n-1}}$

• Characteristic Deflection,

• $D_c = \bar{D} + 2\sigma$ for important roads to cover 97.7% deflection values,

• $D_c = \bar{D} + \sigma$ for low traffic roads, to cover 84.1% deflection values

* Corrections

→ Temperature correction factor +0.0065 mm per °C for pavement temperature below 35°C and -0.0065 mm per °C for pavement temperature above 35°C

→ Tentative correction factor of 2 for clayed soil and 1.3 for sandy soil if the measurements were taken during dry conditions.

* IRC formula of Overlay Thickness

$$\rightarrow h_o = 550 \log_{10} \left[\frac{D_c}{D_a} \right]$$

→ $D_a = 1.0, 1.25$ and 1.5 mm if the projected traffic is 1500-4500, 450-1500 and 150-250 vpd respectively

$$\text{where, } A = P [1 + \alpha]^{n+y}$$

when bituminous concrete is used, equivalency factor of 2 be used.

* Overlay Design-Example

Benkelman beam deflection studies were carried out on 10 selected points on a stretch of flexible pavement during summer. The deflection values obtained in mm are as below. If the present traffic consists of 800 commercial vehicles per day (CVPD), determine the thickness of bituminous overlay required. The pavement temperature during test was 30°C, and the soil type is sandy subgrade soil. Assume annual rate of growth of traffic as 7.5%. Design life 5 years, construction period 6 months.

S.No.	Dial Gauge Reading		
	Initial	Intermediate	Final
1	0	0.54	0.56
2	0	0.54	0.54
3	0	0.50	0.51
4	0	0.53	0.53
5	0	0.48	0.49
6	0	0.46	0.49
7	0	0.50	0.51
8	0	0.57	0.57
9	0	0.54	0.56
10	0	0.53	0.54

SN	DGL			D ₀ - D _i	D ₀ - D _f	Check (D ₀ - D _i) - (D ₀ - D _f), mm	Deflection (mm)
	D ₀	D _i	D _f				
1	0	0.54	0.56	-0.54	-0.56	0.02 < 0.025	0.56 × 2 = 1.12
2	0	0.54	0.54	-0.54	-0.54	0.00 < 0.025	0.54 × 2 = 1.08
3	0	0.50	0.51	-0.50	-0.51	0.01 < 0.025	0.51 × 2 = 1.02
4	0	0.53	0.53	-0.53	-0.53	0.00 < 0.025	0.53 × 2 = 1.06
5	0	0.48	0.49	-0.48	-0.49	0.01 < 0.025	0.49 × 2 = 0.98
6	0	0.46	0.49	-0.46	-0.49	0.03 > 0.025	0.49 × 2 + 2 × 2.91 × (0.49 - 0.46) = 1.855
7	0	0.50	0.51	-0.50	-0.51	0.01 < 0.025	0.51 × 2 = 1.02
8	0	0.57	0.57	-0.57	-0.57	0.00 < 0.025	0.57 × 2 = 1.14
9	0	0.54	0.56	-0.54	-0.56	0.02 < 0.025	0.56 × 2 = 1.12
10	0	0.53	0.54	-0.53	-0.54	0.01 < 0.025	0.54 × 2 = 1.08

Mean deflection:

$$\bar{D} = \frac{\sum D}{n} = \frac{1.12 + 1.08 + 1.02 + \dots + 1.12 + 1.08}{10} = 1.0775 \text{ mm}$$

Standard deviation:

$$\sum (D - \bar{D})^2 = (1.12 - 1.0775)^2 + (1.08 - 1.0775)^2 + \dots + (1.08 - 1.0775)^2 = 0.0299$$

$$\sigma = \sqrt{\frac{\sum (D - \bar{D})^2}{n-1}} = \sqrt{\frac{0.0299}{10-1}} = 0.0576$$

$$\text{Characteristic deflection} = 1.0775 + 2(0.0576) = 1.1922 \text{ mm}$$

• Correction for temperature:

Test Temp = 30°C

Correction for temperature = $0.065(35-30) = 0.0325\text{mm}$

Characteristic deflection after temp correction
= $1.1927 + 0.0325 = 1.2252\text{mm}$.

• Correction for Moisture:

Sandy subgrade:

Correction for Moisture = 1.3

Characteristic deflection after correction for moisture
= 1.3×1.2252
= 1.5928mm .

• Traffic volume at the end of design period

$$A = P(1+r)^{n+1}$$

$$= 800 [1 + 0.075]^{1/2 \times 5} = 1191 \text{ veh/day}$$

• IRC formula for overlay:

$$h_o = 550 \log_{10} \frac{D_c}{D_a}$$

$D_a = 1$ for Traffic (1500-4500 vpd),

1.25 for (450-1500 vpd.)

$$h_o = 550 \log_{10} \frac{1.5928}{1.25} = 57.889 \approx 58\text{mm}$$

Thickness in terms of DBM/AC = $\frac{58}{2} = \underline{\underline{29\text{mm}}}$